



The following excerpt are pages from the North American Product Technical Guide, Volume 2: Anchor Fastening, Edition 19.

Please refer to the publication in its entirety for complete details on this product including data development, product specifications, general suitability, installation, corrosion and spacing and edge distance guidelines.

US&CA: <https://submittals.us.hilti.com/PTGVol2/>

To consult directly with a team member regarding our anchor fastening products, contact Hilti's team of technical support specialists between the hours of 7:00am – 6:00pm CST.






US: 877-749-6337 or [HNATechnicalServices@hilti.com](mailto:HNATechnicalServices@hilti.com)

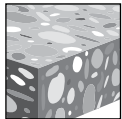
CA: 1-800-363-4458, ext. 6 or [CATechnicalServices@hilti.com](mailto:CATechnicalServices@hilti.com)

### 3.3.8 KWIK Bolt 3 CARBON AND STAINLESS STEEL SCREW ANCHOR

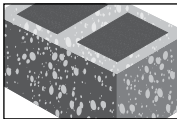
#### PRODUCT DESCRIPTION

##### KWIK Bolt 3 carbon steel, stainless steel anchors, and hot-dipped galvanized plating

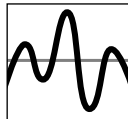
Anchor System			Features and Benefits
 Carbon Steel KB3	 Hot Dipped Galvanized KB3	 Stainless Steel KB3	<ul style="list-style-type: none"> <li>Used with Hilti Dust Removal System (DRS) for dustless drilling and installation (compliant with Table 1 of OSHA 1926.1153 regulations for silica dust exposure).</li> <li>Accurate SafeSet™ installation when using the Hilti SIW-6AT-A22 impact wrench and the SI-AT-A22 Adaptive Torque Module</li> <li>Length identification code facilitates quality control and inspection after installation.</li> <li>Through fixture installation and variable thread lengths improve productivity and accommodate various base plate thicknesses.</li> <li>Raised impact section (Dog Point) prevents thread damage during installation.</li> <li>Anchor size is same as drill bit size for easy installation. For temporary applications anchors may be driven into drilled holes after usage.</li> <li>Mechanical expansion allows immediate load application.</li> <li>Can be installed with innovative Hilti Torque Bar in conjunction with Hilti impact tools.</li> </ul>
 Hilti SIW-6AT-A22 impact wrench and the SI-AT-A22 Adaptive Torque Module	 S-TB torque bar   A-18/A22 impact tool		



Uncracked concrete



Grout-filled concrete masonry



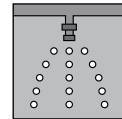
Seismic design categories A-F



Hollow drill bit adaptive torque tool (AT)



Profis Anchor design software



Fire sprinkler listings

Approvals/Listings	
ICC-ES (International Code Council) 2015 International Building Code / International Residential Code (IBC/IRC)	ESR-2302 in concrete per ACI 318-14 Ch. 17 / ACI 355.2/ ICC-ES AC193 ESR-1385 in grout-filled CMU per ICC-ES AC58
City of Los Angeles	City of Los Angeles 2017 LABC Supplement (within ESR-2032) RR 25577M in grout-filled CMU
Florida Building Code	2010 FBC with HVHZ
FM (Factory Mutual)	Pipe hanger components for automatic sprinkler systems 3/8 through 3/4
UL and cUL (Underwriters Laboratory)	Pipe hanger equipment for fire protection services for 3/8 through 3/4
Nuclear Quality Assurance	Qualified under NQA-1 Nuclear Quality Program



## MATERIAL SPECIFICATIONS

### Carbon steel with electroplated zinc

All carbon steel KWIK Bolt 3 and Rod Coupling Anchors, excluding the 3/4 x 12 and 1-inch diameter sizes, have the tensile bolt fracture loads shown in table 1.

All carbon steel 3/4 x 12 and 1 inch diameter sizes and carbon steel KWIK Bolt 3 Countersunk anchor bodies have mechanical properties as listed in table 1.

Carbon steel anchor components plated in accordance with ASTM B633 to a minimum thickness of 5 µm.

Nuts conform to the requirements of ASTM A563, Grade A, Hex.

Washers meet the requirements of ASTM F844.

Expansion wedges are manufactured from carbon steel, except the following anchors have stainless steel wedges:

- All 1/4-inch diameter anchors
- 3/4x12
- All 1-inch diameter anchors
- All KWIK Bolt 3 Countersunk

### Carbon steel with hot-dip galvanized plating

Anchor bodies manufactured from carbon steel have the tensile bolt fracture loads shown in table 1.

Carbon steel anchor components have an average zinc plating thickness greater than 43 µm according to ASTM A153, Class C.

Nuts conform to the requirements of ASTM A563, Grade A, Hex.

Washers meet the requirements of ASTM F844.

Stainless steel expansion wedges are manufactured from either AISI Type 304 or Type 316.

### Stainless steel

Anchor bodies smaller than 3/4-inch, excluding all KWIK Bolt 3 Countersunk, are produced from AISI Type 304 or Type 316 stainless steel having the bolt fracture loads shown in table 1.

Anchor bodies 3/4-inch and larger, and all stainless steel KWIK Bolt 3 Countersunk anchor bodies, are produced from AISI Type 304 or Type 316 stainless steel having the mechanical properties shown in table 1.

Nuts meet the dimensional requirements of ASTM F594.

Washers meet the dimensional requirements of ANSI B18.22.1, Type A, plain.

Stainless steel expansion wedges for AISI Type 304 are made from either AISI Type 304 or Type 316. Stainless steel expansion wedges for AISI Type 316 anchors are made from type 316. All stainless steel nuts and washers for AISI Type 304 or Type 316 anchors are manufactured from AISI Type 304 or 316, respectively.

**Table 1 - Hilti KWIK Bolt 3 Bolt fracture load (lb)<sup>1</sup>**

Nominal anchor diameter in.	Carbon steel	Hot-dip galvanized	Stainless steel
1/4	2,900	no offering	2,900
3/8	7,200	no offering	7,200
1/2	12,400	12,400	12,400
5/8	19,600	19,600	21,900
3/4	28,700	28,700	$f_{uta} \geq 76, f_{ya} \geq 64^2$
1	$f_{uta} \geq 88, f_{ya} \geq 75^2$	no offering	$f_{uta} \geq 76, f_{ya} \geq 64^2$

<sup>1</sup> Bolt fracture loads are determined by testing in a universal tensile machine for quality control at the manufacturing facility. These loads are not intended for design use. See tables 4 and 12 for the steel design strengths of carbon steel and stainless steel, respectively.

<sup>2</sup> All 3/4-in. stainless steel, 3/4x12 carbon steel, all 1-in. carbon steel and all 1-in. stainless steel material strengths specified by the tensile and yield strengths expressed in (ksi). Bolt fracture loads not applicable for these models.

## INSTALLATION PARAMETERS

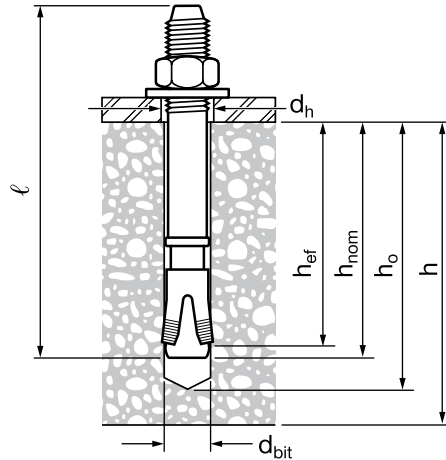


Figure 1 - KWIK Bolt 3 installation

Table 2 - Hilti KWIK Bolt 3 specifications

Setting information	Symbol	Units	Nominal anchor diameter									
			1/4	3/8	1/2	5/8	3/4	1				
Drill bit dia.	$d_{bit}$	in.	1/4	3/8	1/2	5/8	3/4	1				
Minimum nominal embedment	$h_{nom}$	in. (mm)	1-3/4 (44)	2-3/8 (60)	2-1/4 (57)	3-5/8 (92)	3-1/2 (89)	4-3/8 (111)	4-1/4 (108)	5-5/8 (143)	4-5/8 117	6-3/8 162
Minimum effective embedment	$h_{ef}$	in. (mm)	1-1/2 (38)	2 (51)	2 (51)	3-1/4 (83)	3-1/8 (79)	4 (102)	3-3/4 (95)	5 (127)	4 (102)	5-3/4 (146)
Minimum hole depth	$h_o$	in. (mm)	2 (51)	2-5/8 (67)	2-5/8 (67)	4 (102)	3-7/8 (98)	4-3/4 (121)	4-1/2 (114)	5-3/4 (146)	5 (127)	6-3/4 (171)
Fixture hole dia.	$d_h$	in.	5/16	7/16	9/16	11/16	13/16	1				
Anchor length	$l$		See ordering information									
Installation torque concrete	$T_{inst}$	ft-lb (Nm)	4 (5)	20 (27)	40 (54)	60 (81)	110 (149)	150 (203)				
Installation torque masonry	$T_{inst}$	ft-lb (Nm)	4 (5)	15 (20)	25 (34)	65 (88)	120 (163)	not recommended				
Wrench size		in.	7/16	9/16	3/4	15/16	1-1/8	1-1/2				

<sup>1</sup> For more information, see ESR-1385 and section 3.3.8.3.3. Approval value are for carbon steel anchors only.

## DESIGN INFORMATION IN CONCRETE PER ACI 318.14

### ACI 318-14 Chapter 17 design

The load values contained in this section are Hilti Simplified Design Tables. The load tables in this section were developed using the Strength Design parameters and variables of ESR-2302 and the equations within ACI 318-14 Chapter 17. For a detailed explanation of the Hilti Simplified Design Tables, refer to section 3.1.7. Data tables from ESR-2302 are not contained in this section, but can be found at [www.icc-es.org](http://www.icc-es.org) or at [www.hilti.com](http://www.hilti.com).

Allowable Stress Design or ASD technical information and data tables can be found at [www.hilti.com](http://www.hilti.com).

**Table 3 - Hilti KWIK Bolt 3 carbon steel strength with concrete / pullout failure in uncracked concrete<sup>1,2,3,4,5</sup>**

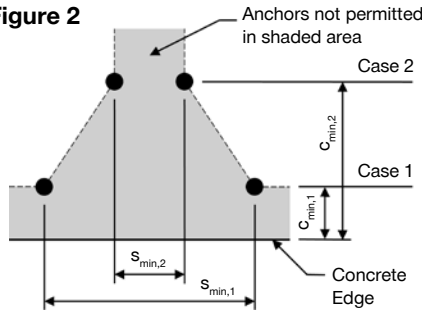
Nominal anchor diameter in.	Effective embed. in. (mm)	Nominal embed. in. (mm)	Tension - $\phi N_n$				Shear - $\phi V_n$			
			$f'_c = 2,500$ psi lb (kN)	$f'_c = 3,000$ psi lb (kN)	$f'_c = 4,000$ psi lb (kN)	$f'_c = 6,000$ psi lb (kN)	$f'_c = 2,500$ psi lb (kN)	$f'_c = 3,000$ psi lb (kN)	$f'_c = 4,000$ psi lb (kN)	$f'_c = 6,000$ psi lb (kN)
1/4	1-1/2 (38)	1-3/4 (44)	1,025 (4.6)	1,080 (4.8)	1,180 (5.2)	1,330 (5.9)	1,545 (6.9)	1,690 (7.5)	1,950 (8.7)	2,390 (10.6)
	2 (51)	2-3/8 (60)	2,205 (9.8)	2,415 (10.7)	2,790 (12.4)	3,420 (15.2)	2,375 (10.6)	2,605 (11.6)	3,005 (13.4)	3,680 (16.4)
1/2	2 (51)	2-1/4 (57)	2,205 (9.8)	2,415 (10.7)	2,790 (12.4)	3,420 (15.2)	2,375 (10.6)	2,605 (11.6)	3,005 (13.4)	3,680 (16.4)
	3-1/4 (83)	3-1/2 (89)	4,420 (19.7)	4,840 (21.5)	5,590 (24.9)	6,845 (30.4)	9,845 (43.8)	10,785 (48.0)	12,450 (55.4)	15,250 (67.8)
5/8	3-1/8 (79)	3-1/2 (89)	4,310 (19.2)	4,720 (21.0)	5,450 (24.2)	6,675 (29.7)	9,280 (41.3)	10,165 (45.2)	11,740 (52.2)	14,380 (64.0)
	4 (102)	4-3/8 (111)	6,240 (27.8)	6,835 (30.4)	7,895 (35.1)	9,665 (43.0)	13,440 (59.8)	14,725 (65.5)	17,000 (75.6)	20,820 (92.6)
3/4	3-3/4 (95)	4-1/4 (108)	5,665 (25.2)	6,205 (27.6)	7,165 (31.9)	8,775 (39.0)	12,200 (54.3)	13,365 (59.5)	15,430 (68.6)	18,900 (84.1)
	5 (127)	5-5/8 (143)	6,880 (30.6)	7,535 (33.5)	8,705 (38.7)	10,660 (47.4)	18,785 (83.6)	20,575 (91.5)	23,760 (105.7)	29,100 (129.4)

- 1 See section 3.1.8 to convert design strength value to ASD value.
- 2 Linear interpolation between embedment depths and concrete compressive strengths is not permitted.
- 3 Apply spacing, edge distance, and concrete thickness factors in tables 6 to 10 as necessary. Compare to steel values in table 4. The lesser of the values is to be used for the design.
- 4 Tabular values are for normal weight concrete only. For lightweight concrete multiply design strength by  $\lambda_a$  as follows: for sand-lightweight,  $\lambda_a = 0.68$ ; for all-lightweight,  $\lambda_a = 0.60$
- 5 Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete.

**Table 4 - Steel design strength for Hilti KWIK Bolt 3 carbon steel anchors<sup>1,2</sup>**

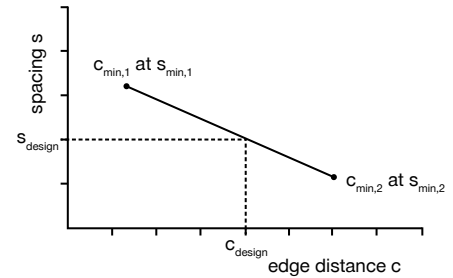
Nominal anchor diameter in.	Nominal embedment in. (mm)	Tensile <sup>3</sup> $\phi N_{sa}$ lb (kN)	Shear <sup>4</sup> $\phi V_{sa}$ lb (kN)
1/4	1-3/4 (44)	1,590 (7.1)	1,065 (4.7)
	2-3/8 (60)	4,770 (21.2)	2,905 (12.9)
1/2	2-1/4 (57)	8,745 (38.9)	4,315 (19.2)
	3-1/2 (89)		4,390 (19.5)
5/8	3-1/2 (89)	13,515 (60.1)	7,950 (35.4)
	4-3/8 (111)		
3/4	4-1/4 (108)	19,080 (84.9)	10,180 (45.3)
	5-5/8 (143)		10,785 (48.0)

- 1 See section 3.1.8 to convert design strength value to ASD value.
- 2 KWIK Bolt 3 carbon steel anchors are to be considered ductile steel elements.
- 3 Tensile  $\phi N_{sa} = \phi A_{se,N} f_{uta}$  as noted in ACI 318-14 Chapter 17.
- 4 Shear values determined by static shear tests with  $\phi V_{sa} < \phi 0.60 A_{se,V} f_{uta}$  as noted in ACI 318-14 Chapter 17.

**Figure 2**


For a specific edge distance, the permitted spacing is calculated as follows:

$$s \geq s_{\min,2} + \frac{(s_{\min,1} - s_{\min,2})}{(c_{\min,1} - c_{\min,2})} (c - c_{\min,2})$$


**Table 5 - Carbon steel Hilti KWIK Bolt 3 installation parameters<sup>1</sup>**

Setting information	Symbol	Units	Nominal anchor diameter d <sub>o</sub>												
			1/4	3/8		1/2		5/8		3/4					
Effective minimum embedment	$h_{ef}$	in. (mm)	1-1/2 (38)	2 (51)	2 (51)	3-1/4 (83)	3-1/8 (79)	4 (102)	3-3/4 (95)	5 (127)					
Minimum member thickness	$h_{min}$	in. (mm)	4 (102)	4 (102)	5 (127)	4 (102)	5 (127)	6 (152)	8 (203)	5 (127)	6 (152)	8 (203)	6 (152)	8 (203)	8 (203)
Case 1	$c_{\min,1}$	in. (mm)	1-3/8 (35)	2 (51)	1-1/2 (38)	2-1/8 (54)	2 (51)	1-5/8 (41)	1-5/8 (41)	2-1/4 (57)	1-3/4 (44)	1-3/4 (44)	2-3/4 (70)	2-5/8 (67)	2-1/2 (64)
	for $s_{\min,1} \geq$	in. (mm)	1-3/4 (44)	2-7/8 (73)	3-1/2 (89)	4-7/8 (124)	4-3/4 (121)	4-1/4 (108)	4 (102)	5-1/4 (133)	4-3/4 (121)	4 (102)	6-7/8 (175)	6-1/2 (165)	6-3/8 (162)
Case 2	$c_{\min,2}$	in. (mm)	1-5/8 (41)	2-3/8 (60)	2-3/8 (60)	2-5/8 (67)	2-3/8 (60)	2-1/4 (57)	2 (51)	3-1/8 (79)	2-3/8 (60)	2-1/4 (57)	3-3/4 (95)	3-3/8 (86)	3-3/8 (86)
	for $s_{\min,2} \geq$	in. (mm)	1-1/4 (32)	1-3/4 (44)	1-3/4 (44)	2-1/2 (64)	2-1/4 (57)	2 (51)	1-7/8 (48)	2-3/8 (60)	2-1/8 (54)	2-1/8 (54)	3-3/4 (95)	3-3/8 (86)	3-1/4 (83)

<sup>1</sup> Linear interpolation is permitted to establish an edge distance and spacing combination between Case 1 and Case 2. Linear interpolation for a specific edge distance c, where  $c_{\min,1} < c < c_{\min,2}$  will determine the permissible spacings.

**Table 6 - Load adjustment factors for 1/4-in. diameter Hilti KWIK Bolt 3 carbon steel anchor in uncracked concrete<sup>1,2</sup>**

1/4-in. KB3 carbon steel uncracked concrete	Spacing factor in tension $f_{AN}$	Edge distance factor in tension $f_{RN}$	Spacing factor in shear <sup>3</sup> $f_{AV}$	Edge distance in shear		Concrete thickness factor in shear <sup>4</sup> $f_{HV}$
				⊥ toward edge $f_{RV}$	∥ To and away from edge $f_{RV}$	
Embedment $h_{nom}$ in. (mm)	1-3/4 (44)	1-3/4 (44)	1-3/4 (44)	1-3/4 (44)	1-3/4 (44)	1-3/4 (44)
Spacing (s) / Edge Distance (c <sub>o</sub> ) / Concrete Thickness (h) - in. (mm)	1-1/4 (32)	0.64	n/a	0.56	n/a	n/a
	1-3/8 (35)	0.65	0.58	0.57	0.26	0.51
	1-1/2 (38)	0.67	0.61	0.57	0.29	0.58
	2 (51)	0.72	0.75	0.60	0.45	0.75
	3 (76)	0.83	1.00	0.65	0.83	1.00
	3-1/2 (89)	0.89		0.67	1.00	
	4 (102)	0.94		0.70		0.88
	4-1/2 (114)	1.00		0.72		0.94
	5 (127)			0.74		0.99
	5-1/2 (140)			0.77		1.00
	6 (152)			0.79		
7 (178)			0.84			
8 (203)			0.89			
9 (229)			0.94			
10 (254)			0.99			
11 (279)			1.00			

<sup>1</sup> Linear interpolation not permitted.  
<sup>2</sup> When combining multiple load adjustment factors (e.g. for a 4 anchor pattern in a corner with thin concrete member) the design can become very conservative. To optimize the design, use Hilti PROFIS Anchor Design software or perform anchor calculation using design equations from ACI 318-14 Chapter 17.  
<sup>3</sup> Spacing factor reduction in shear,  $f_{AV}$ , assumes an influence of a nearby edge. If no edge exists, then  $f_{AV} = f_{AN}$ .  
<sup>4</sup> Concrete thickness reduction factor in shear,  $f_{HV}$ , assumes an influence of a nearby edge. If no edge exists, then  $f_{HV} = 1.0$ .  
 If a reduction factor value is in a shaded cell, this indicates that this specific edge distance may not be permitted with a certain spacing (or vice versa). Check with table 5 and figure 2 of this section to calculate permissible edge distance, spacing and concrete thickness combinations. Use of Hilti KWIK Bolt 3 anchors with edge distance and spacing dimensions smaller than what is noted in this table is permitted.

**Table 7 - Load adjustment factors for 3/8-in. diameter Hilti KWIK Bolt 3 carbon steel anchor in uncracked concrete<sup>1,2</sup>**

3/8-in. KB3 carbon steel uncracked concrete	Spacing factor in tension $f_{AN}$	Edge distance factor in tension $f_{RN}$		Spacing factor in shear <sup>3</sup> $f_{AV}$	Edge distance in shear		Concrete thickness factor in shear <sup>4</sup> $f_{HV}$
					⊥ Toward edge $f_{RV}$	To and away from edge $f_{RV}$	
Embedment $h_{nom}$ in. (mm)	2-3/8 (60)	2-3/8 (60)	2-3/8 (60)	2-3/8 (60)	2-3/8 (60)	2-3/8 (60)	2-3/8 (60)
Spacing (s) / edge distance (c <sub>g</sub> ) / concrete thickness (h) - in. (mm)	1-3/4 (44)	0.65	n/a	0.57	n/a	n/a	n/a
	2 (51)	0.67	0.50	0.58	0.35	0.50	n/a
	2-1/2 (64)	0.71	0.58	0.60	0.49	0.58	n/a
	3 (76)	0.75	0.67	0.62	0.64	0.67	n/a
	3-1/4 (83)	0.77	0.72	0.63	0.72	0.72	n/a
	3-1/2 (89)	0.79	0.78	0.64	0.81	0.81	n/a
	4 (102)	0.83	0.89	0.67	0.99	0.99	0.81
	4-1/2 (114)	0.88	1.00	0.69	1.00	1.00	0.86
	5 (127)	0.92		0.71			0.91
	6 (152)	1.00		0.75			1.00
	7 (178)			0.79			
	8 (203)			0.83			
9 (229)			0.87				
10 (254)			0.91				
11 (279)			0.95				
12 (305)			1.00				

3.3.8

**Table 8 - Load adjustment factors for 1/2-in. diameter Hilti KWIK Bolt 3 carbon steel anchor in uncracked concrete<sup>1,2</sup>**

1/2-in. KB3 carbon steel uncracked concrete	Spacing factor in tension $f_{AN}$		Edge distance factor in tension $f_{RN}$		Spacing factor in shear <sup>3</sup> $f_{AV}$		Edge distance in shear				Concrete thickness factor in shear <sup>4</sup> $f_{HV}$		
							⊥ Toward edge $f_{RV}$		To and away from edge $f_{RV}$				
Embedment $h_{nom}$ in. (mm)	2-1/4 (57)	3-1/2 (89)	2-1/4 (57)	3-1/2 (89)	2-1/4 (57)	3-1/2 (89)	2-1/4 (57)	3-1/2 (89)	2-1/4 (57)	3-1/2 (89)	2-1/4 (57)	3-1/2 (89)	
Spacing (s) / edge distance (c <sub>g</sub> ) / concrete thickness (h) - in. (mm)	1-5/8 (41)	n/a	n/a	n/a	0.39	n/a	n/a	n/a	0.07	n/a	0.15	n/a	n/a
	2 (51)	n/a	0.60	n/a	0.42	n/a	0.54	n/a	0.10	n/a	0.20	n/a	n/a
	2-1/8 (54)	n/a	0.61	0.48	0.43	n/a	0.54	0.42	0.11	0.48	0.22	n/a	n/a
	2-1/2 (64)	0.71	0.63	0.54	0.47	0.61	0.55	0.53	0.14	0.54	0.28	n/a	n/a
	3 (76)	0.75	0.65	0.62	0.52	0.63	0.55	0.70	0.19	0.70	0.37	n/a	n/a
	3-1/2 (89)	0.79	0.68	0.72	0.57	0.65	0.56	0.88	0.23	0.88	0.47	n/a	n/a
	4 (102)	0.83	0.71	0.82	0.62	0.68	0.57	1.00	0.29	1.00	0.57	0.84	n/a
	4-1/2 (114)	0.88	0.73	0.92	0.68	0.70	0.58		0.34		0.68	0.89	n/a
	5 (127)	0.92	0.76	1.00	0.74	0.72	0.59		0.40		0.74	0.94	n/a
	6 (152)	1.00	0.81		0.89	0.76	0.61		0.53		0.89	1.00	0.66
	7 (178)		0.86		1.00	0.81	0.63		0.66		1.00		0.71
	8 (203)		0.91			0.85	0.64		0.81				0.76
	9 (229)		0.96			0.89	0.66		0.97				0.81
	10 (254)		1.00			0.94	0.68		1.00				0.85
	11 (279)					0.98	0.70						0.89
	12 (305)					1.00	0.72						0.93
	14 (356)						0.75						1.00
	16 (406)						0.79						
	18 (457)						0.83						
20 (508)						0.86							
> 24 (610)						0.93							

- Linear interpolation not permitted.
  - When combining multiple load adjustment factors (e.g. for a 4 anchor pattern in a corner with thin concrete member) the design can become very conservative. To optimize the design, use Hilti PROFIS Anchor Design software or perform anchor calculation using design equations from ACI 318-14 Chapter 17.
  - Spacing factor reduction in shear,  $f_{AV}$ , assumes an influence of a nearby edge. If no edge exists, then  $f_{AV} = f_{AN}$ .
  - Concrete thickness reduction factor in shear,  $f_{HV}$ , assumes an influence of a nearby edge. If no edge exists, then  $f_{HV} = 1.0$ .
- ☐ If a reduction factor value is in a shaded cell, this indicates that this specific edge distance may not be permitted with a certain spacing (or vice versa). Check with table 5 and figure 2 of this section to calculate permissible edge distance, spacing and concrete thickness combinations. Use of Hilti KWIK Bolt 3 anchors with edge distance and spacing dimensions smaller than what is noted in this table is permitted.

**Table 9 - Load adjustment factors for 5/8-in. diameter Hilti KWIK Bolt 3 carbon steel anchor in uncracked concrete<sup>1,2</sup>**

5/8-in. KB3 carbon steel uncracked concrete		Spacing factor in tension $f_{AN}$		Edge distance factor in tension $f_{RN}$		Spacing factor in shear <sup>3</sup> $f_{AV}$		Edge distance in shear				Conc. thickness factor in shear <sup>4</sup> $f_{HV}$	
								⊥ toward edge $f_{RV}$		to and away from edge $f_{RV}$			
Embedment $h_{nom}$	in. (mm)	3-1/2 (89)	4-3/8 (111)	3-1/2 (89)	4-3/8 (111)	3-1/2 (89)	4-3/8 (111)	3-1/2 (89)	4-3/8 (111)	3-1/2 (89)	4-3/8 (111)	3-1/2 (89)	4-3/8 (111)
Spacing (s) / edge distance ( $c_e$ ) / concrete thickness (h) - in. (mm)	1-3/4 (44)	n/a	n/a	n/a	0.32	n/a	n/a	n/a	0.07	n/a	0.14	n/a	n/a
	2 (51)	n/a	n/a	n/a	0.34	n/a	n/a	n/a	0.08	n/a	0.17	n/a	n/a
	2-1/8 (54)	n/a	0.59	n/a	0.34	n/a	0.53	n/a	0.09	n/a	0.18	n/a	n/a
	2-1/4 (57)	n/a	0.59	0.39	0.35	n/a	0.54	0.14	0.10	0.27	0.20	n/a	n/a
	2-3/8 (60)	0.63	0.60	0.40	0.36	0.55	0.54	0.15	0.11	0.30	0.21	n/a	n/a
	2-1/2 (64)	0.63	0.60	0.41	0.37	0.55	0.54	0.16	0.12	0.32	0.23	n/a	n/a
	3 (76)	0.66	0.63	0.46	0.40	0.56	0.55	0.21	0.15	0.42	0.30	n/a	n/a
	4 (102)	0.71	0.67	0.55	0.47	0.58	0.56	0.32	0.23	0.55	0.47	n/a	n/a
	5 (127)	0.77	0.71	0.67	0.55	0.60	0.58	0.45	0.33	0.67	0.55	0.63	n/a
	6 (152)	0.82	0.75	0.80	0.63	0.62	0.59	0.59	0.43	0.80	0.63	0.69	0.62
	7 (178)	0.87	0.79	0.93	0.74	0.64	0.61	0.75	0.54	0.93	0.74	0.74	0.67
	8 (203)	0.93	0.83	1.00	0.84	0.66	0.63	0.91	0.66	1.00	0.84	0.79	0.71
	9 (229)	0.98	0.88		0.95	0.68	0.64	1.00	0.79		0.95	0.84	0.75
	10 (254)	1.00	0.92		1.00	0.70	0.66		0.92		1.00	0.89	0.80
	11 (279)		0.96			0.72	0.67		1.00			0.93	0.83
	12 (305)		1.00			0.74	0.69					0.97	0.87
	14 (356)					0.77	0.72					1.00	0.94
	16 (406)					0.81	0.75						1.00
18 (457)					0.85	0.78							
20 (508)					0.89	0.82							
24 (610)					0.97	0.88							
> 30 (762)					1.00	0.97							

**Table 10 - Load adjustment factors for 3/4-in. diameter Hilti KWIK Bolt 3 carbon steel anchor in uncracked concrete<sup>1,2</sup>**

3/4-in. KB3 carbon steel uncracked concrete		Spacing factor in tension $f_{AN}$		Edge distance factor in tension $f_{RN}$		Spacing factor in shear <sup>3</sup> $f_{AV}$		Edge distance in shear				Conc. thickness factor in shear <sup>4</sup> $f_{HV}$	
								⊥ toward edge $f_{RV}$		to and away from edge $f_{RV}$			
Embedment $h_{nom}$	in. (mm)	4-1/4 (108)	5-1/2 (140)	4-1/4 (108)	5-1/2 (140)	4-1/4 (108)	5-1/2 (140)	4-1/4 (108)	5-1/2 (140)	4-1/4 (108)	5-1/2 (140)	4-1/4 (108)	5-1/2 (140)
Spacing (s) / edge distance ( $c_e$ ) / concrete thickness (h) - in. (mm)	2-1/2 (64)	n/a	n/a	n/a	0.42	n/a	n/a	n/a	0.09	n/a	0.18	n/a	n/a
	2-3/4 (70)	n/a	n/a	0.36	0.44	n/a	n/a	0.15	0.11	0.31	0.21	n/a	n/a
	3 (76)	n/a	n/a	0.38	0.45	n/a	n/a	0.17	0.12	0.35	0.24	n/a	n/a
	3-1/4 (83)	n/a	0.61	0.40	0.47	n/a	0.54	0.20	0.14	0.39	0.27	n/a	n/a
	3-1/2 (89)	n/a	0.62	0.41	0.49	n/a	0.55	0.22	0.15	0.41	0.30	n/a	n/a
	3-3/4 (95)	0.67	0.63	0.43	0.50	0.57	0.55	0.24	0.17	0.43	0.34	n/a	n/a
	4 (102)	0.68	0.63	0.45	0.52	0.57	0.55	0.27	0.18	0.45	0.37	n/a	n/a
	4-1/2 (114)	0.70	0.65	0.49	0.56	0.58	0.56	0.32	0.22	0.49	0.44	n/a	n/a
	5 (127)	0.72	0.67	0.53	0.59	0.59	0.57	0.38	0.26	0.53	0.52	n/a	n/a
	6 (152)	0.77	0.70	0.62	0.67	0.60	0.58	0.49	0.34	0.62	0.67	0.65	n/a
	7 (178)	0.81	0.73	0.72	0.75	0.62	0.59	0.62	0.43	0.72	0.75	0.70	n/a
	8 (203)	0.86	0.77	0.82	0.84	0.64	0.61	0.76	0.52	0.82	0.84	0.75	0.66
	9 (229)	0.90	0.80	0.92	0.95	0.66	0.62	0.91	0.62	0.92	0.95	0.79	0.70
	10 (254)	0.94	0.83	1.00	1.00	0.67	0.64	1.00	0.73	1.00	1.00	0.83	0.74
	11 (279)	0.99	0.87			0.69	0.65		0.84			0.87	0.77
	12 (305)	1.00	0.90			0.71	0.66		0.96			0.91	0.81
	14 (356)		0.97			0.74	0.69		1.00			0.99	0.87
	16 (406)		1.00			0.78	0.72					1.00	0.93
18 (457)					0.81	0.74						0.99	
20 (508)					0.85	0.77						1.00	
24 (610)					0.92	0.82							
30 (762)					1.00	0.91							
> 36 (914)						0.99							

1 Linear interpolation not permitted.

2 When combining multiple load adjustment factors (e.g. for a 4 anchor pattern in a corner with thin concrete member) the design can become very conservative. To optimize the design, use Hilti PROFIS Anchor Design software or perform anchor calculation using design equations from ACI 318-14 Chapter 17.

3 Spacing factor reduction in shear,  $f_{AV}$ , assumes an influence of a nearby edge. If no edge exists, then  $f_{AV} = f_{AN}$ .

4 Concrete thickness reduction factor in shear,  $f_{HV}$ , assumes an influence of a nearby edge. If no edge exists, then  $f_{HV} = 1.0$ .

If a reduction factor value is in a shaded cell, this indicates that this specific edge distance may not be permitted with a certain spacing (or vice versa). Check with table 5 and figure 2 of this section to calculate permissible edge distance, spacing and concrete thickness combinations. Use of Hilti KWIK Bolt 3 anchors with edge distance and spacing dimensions smaller than what is noted in this table is permitted.



**Table 11 - Hilti KWIK Bolt 3 stainless steel design strength with concrete / pullout failure in uncracked concrete<sup>1,2,3,4,5</sup>**

Nominal anchor diameter in.	Effective embed. in. (mm)	Nominal embed. in. (mm)	Tension - $\phi N_n$				Shear - $\phi V_n$			
			$f'_c = 2,500$ psi lb (kN)	$f'_c = 3,000$ psi lb (kN)	$f'_c = 4,000$ psi lb (kN)	$f'_c = 6,000$ psi lb (kN)	$f'_c = 2,500$ psi lb (kN)	$f'_c = 3,000$ psi lb (kN)	$f'_c = 4,000$ psi lb (kN)	$f'_c = 6,000$ psi lb (kN)
1/4	1-1/2 (38)	1-3/4 (44)	730 (3.2)	770 (3.4)	840 (3.7)	950 (4.2)	1,545 (6.9)	1,690 (7.5)	1,950 (8.7)	2,390 (10.6)
	3/8	2-3/8 (60)	1,925 (8.6)	2,110 (9.4)	2,440 (10.9)	2,985 (13.3)	2,375 (10.6)	2,605 (11.6)	3,005 (13.4)	3,680 (16.4)
1/2	2 (51)	2-1/4 (57)	2,150 (9.6)	2,355 (10.5)	2,720 (12.1)	3,335 (14.8)	2,375 (10.6)	2,605 (11.6)	3,005 (13.4)	3,680 (16.4)
	3-1/4 (83)	3-1/2 (89)	3,920 (17.4)	4,295 (19.1)	4,960 (22.1)	6,070 (27.0)	9,845 (43.8)	10,785 (48.0)	12,450 (55.4)	15,250 (67.8)
5/8	3-1/8 (79)	3-1/2 (89)	4,050 (18.0)	4,435 (19.7)	5,120 (22.8)	6,275 (27.9)	9,280 (41.3)	10,165 (45.2)	11,740 (52.2)	14,380 (64.0)
	4 (102)	4-3/8 (111)	5,090 (22.6)	5,575 (24.8)	6,440 (28.6)	7,885 (35.1)	13,440 (59.8)	14,725 (65.5)	17,000 (75.6)	20,820 (92.6)
3/4	3-3/4 (95)	4-1/4 (108)	5,560 (24.7)	6,090 (27.1)	7,035 (31.3)	8,615 (38.3)	12,200 (54.3)	13,365 (59.5)	15,430 (68.6)	18,900 (84.1)
	5 (127)	5-1/2 (140)	7,040 (31.3)	7,710 (34.3)	8,905 (39.6)	10,905 (48.5)	18,785 (83.6)	20,575 (91.5)	23,760 (105.7)	29,100 (129.4)
1	4 (102)	4-1/2 (114)	6,240 (27.8)	6,835 (30.4)	7,895 (35.1)	9,665 (43.0)	13,440 (59.8)	14,725 (65.5)	17,000 (75.6)	20,820 (92.6)
	5-3/4 (146)	6-1/4 (159)	10,110 (45.0)	11,070 (49.2)	12,785 (56.9)	15,660 (69.7)	23,165 (103.0)	25,375 (112.9)	29,300 (130.3)	35,885 (159.6)

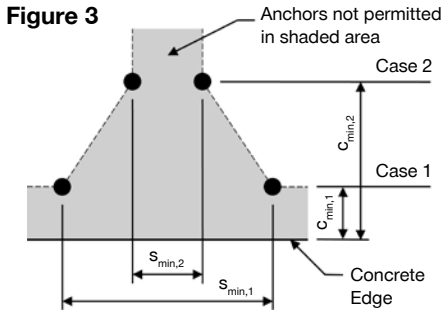
- 1 See section 3.1.8 to convert design strength value to ASD value.
- 2 Linear interpolation between embedment depths and concrete compressive strengths is not permitted.
- 3 Apply spacing, edge distance, and concrete thickness factors in tables 14 to 19 as necessary. Compare to steel values in table 12. The lesser of the values is to be used for the design.
- 4 Tabular values are for normal-weight concrete only. For lightweight concrete multiply design strength by  $\lambda_a$  as follows: for sand-lightweight,  $\lambda_a = 0.68$ ; for all-lightweight,  $\lambda_a = 0.60$
- 5 Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete.

3.3.8

**Table 12 - Steel design strength for Hilti KWIK Bolt 3 stainless steel anchors<sup>1,2</sup>**

Nominal anchor diameter in.	Nominal embedment in. (mm)	Tensile <sup>3</sup> $\phi N_{sa}$ lb (kN)	Shear <sup>4</sup> $\phi V_{sa}$ lb (kN)
1/4	1-3/4 (44)	1,725 (7.7)	1,090 (4.8)
3/8	2-3/8 (60)	5,175 (23.0)	3,235 (14.4)
1/2	2-1/4 (57)	9,490 (42.2)	2,725 (12.1)
	3-1/2 (89)		4,510 (20.1)
5/8	3-1/2 (89)	14,665 (65.2)	5,820 (25.9)
	4-3/8 (111)		9,295 (41.3)
3/4	4-1/4 (108)	16,200 (72.1)	7,735 (34.4)
	5-1/2 (140)		15,305 (68.1)
1	4-1/2 (114)	31,735 (141.2)	8,130 (36.2)
	6-1/4 (159)		17,775 (79.1)

- 1 See section 3.1.8 to convert design strength value to ASD value.
- 2 KWIK Bolt 3 stainless steel anchors are to be considered ductile steel elements.
- 3 Tensile  $\phi N_{sa} = \phi A_{se,N} f_{uta}$  as noted in ACI 318-14 Chapter 17.
- 4 Shear values determined by static shear tests with  $\phi V_{sa} < \phi 0.60 A_{se,V} f_{uta}$  as noted in ACI 318-14 Chapter 17.



For a specific edge distance, the permitted spacing is calculated as follows:

$$s \geq s_{min,2} + \frac{(s_{min,1} - s_{min,2})}{(c_{min,1} - c_{min,2})} (c - c_{min,2})$$

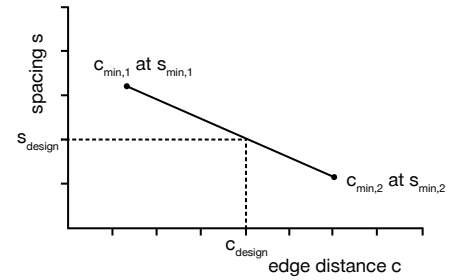


Table 13 - Stainless steel Hilti KWIK Bolt 3 installation parameters<sup>1</sup>

Setting information	Symbol	Units	Nominal anchor diameter d <sub>o</sub>														
			1/4	3/8	1/2		5/8		3/4		1						
Effective minimum embedment	<i>h<sub>ef</sub></i>	in. (mm)	1-1/2 (38)	2 (51)	2 (51)	3-1/4 (83)	3-1/8 (79)	4 (102)	3-3/4 (95)	5 (127)	4 (102)	5-3/4 (146)					
Minimum member thickness	<i>h<sub>min</sub></i>	in. (mm)	4 (102)	4 (102)	5 (127)	4 (102)	6 (152)	6 (152)	8 (203)	5 (127)	6 (152)	8 (203)	8 (203)	8 (203)	10 (254)		
Case 1	<i>c<sub>min,1</sub></i>	in. (mm)	1-3/8 (35)	2 (51)	1-5/8 (41)	2-1/2 (68)	1-7/8 (48)	1-5/8 (41)	1-5/8 (41)	3-1/4 (83)	2-1/2 (64)	2-1/2 (64)	3-1/4 (83)	3 (76)	2-7/8 (73)	3-1/2 (89)	3 (76)
	for <i>s<sub>min,1</sub></i> ≥	in. (mm)	1-3/4 (44)	4 (102)	3-5/8 (92)	5 (127)	4-5/8 (117)	4-1/2 (114)	4-1/4 (108)	5-5/8 (143)	5-1/4 (133)	5 (127)	7 (178)	6-7/8 (175)	6-5/8 (168)	6-3/4 (172)	6-3/4 (172)
Case 2	<i>c<sub>min,2</sub></i>	in. (mm)	1-5/8 (41)	3-1/4 (83)	2-1/2 (64)	2-7/8 (73)	2-3/8 (60)	2-3/8 (60)	2-1/8 (54)	3-7/8 (98)	3 (76)	2-3/4 (70)	4-1/8 (105)	3-3/4 (95)	3-3/4 (95)	4-1/4 (108)	3-3/4 (95)
	for <i>s<sub>min,2</sub></i> ≥	in. (mm)	1-1/4 (32)	2 (51)	1-3/4 (44)	2-1/2 (64)	2-1/4 (57)	2-1/8 (54)	1-7/8 (48)	3-1/8 (79)	2-1/8 (54)	2-1/8 (54)	4 (102)	3-1/2 (89)	3-1/2 (89)	5 (127)	4-3/4 (121)

1 Linear interpolation is permitted to establish an edge distance and spacing combination between Case 1 and Case 2. Linear interpolation for a specific edge distance *c*, where *c<sub>min,1</sub>* < *c* < *c<sub>min,2</sub>* will determine the permissible spacings.

Table 14 - Load adjustment factors for 1/4-in. diameter Hilti KWIK Bolt 3 stainless steel anchor in uncracked concrete<sup>1,2</sup>

1/4-in. KB3 stainless steel uncracked concrete	Spacing factor in tension <i>f<sub>AN</sub></i>	Edge distance factor in tension <i>f<sub>RN</sub></i>	Spacing factor in shear <sup>3</sup> <i>f<sub>AV</sub></i>	Edge distance in shear		Concrete thickness factor in shear <sup>4</sup> <i>f<sub>HV</sub></i>
				⊥ toward edge <i>f<sub>RV</sub></i>	∥ to and away from edge <i>f<sub>RV</sub></i>	
Embedment <i>h<sub>nom</sub></i>	in. (mm)	1-3/4 (44)	1-3/4 (44)	1-3/4 (44)	1-3/4 (44)	1-3/4 (44)
Spacing (s) / edge distance (c <sub>o</sub> ) / concrete thickness (h) - in. (mm)	1-1/4 (32)	0.64	n/a	0.56	n/a	n/a
	1-3/8 (35)	0.65	0.53	0.57	0.26	0.51
	1-1/2 (38)	0.67	0.56	0.57	0.29	0.56
	2 (51)	0.72	0.68	0.60	0.45	0.68
	3 (76)	0.83	1.00	0.65	0.83	1.00
	3-1/2 (89)	0.89		0.67	1.00	
	4 (102)	0.94		0.70		0.88
	4-1/2 (114)	1.00		0.72		0.94
	5 (127)			0.74		0.99
	5-1/2 (140)			0.77		1.00
	6 (152)			0.79		
7 (178)			0.84			
8 (203)			0.89			
9 (229)			0.94			
10 (254)			0.99			
11 (279)			1.00			

1 Linear interpolation not permitted.  
 2 When combining multiple load adjustment factors (e.g. for a 4 anchor pattern in a corner with thin concrete member) the design can become very conservative. To optimize the design, use Hilti PROFIS Anchor Design software or perform anchor calculation using design equations from ACI 318-14 Chapter 17.  
 3 Spacing factor reduction in shear, *f<sub>AV</sub>*, assumes an influence of a nearby edge. If no edge exists, then *f<sub>AV</sub>* = *f<sub>AN</sub>*.  
 4 Concrete thickness reduction factor in shear, *f<sub>HV</sub>*, assumes an influence of a nearby edge. If no edge exists, then *f<sub>HV</sub>* = 1.0.

□ If a reduction factor value is in a shaded cell, this indicates that this specific edge distance may not be permitted with a certain spacing (or vice versa). Check with table 13 and figure 3 of this section to calculate permissible edge distance, spacing and concrete thickness combinations. Use of Hilti KWIK Bolt 3 anchors with edge distance and spacing dimensions smaller than what is noted in this table is permitted.

**Table 15 - Load adjustment factors for 3/8-in. diameter Hilti KWIK Bolt 3 stainless steel anchor in uncracked concrete<sup>1,2</sup>**

3/8-in. KB3 stainless steel uncracked concrete		Spacing factor in tension		Edge distance factor in tension		Spacing factor in shear <sup>3</sup>		Edge distance in shear				Concrete thickness factor in shear <sup>4</sup>	
								⊥ toward edge		to and away from edge			
		$f_{AN}$		$f_{RN}$		$f_{AV}$		$f_{RV}$		$f_{RV}$		$f_{HV}$	
Embedment	in.	2-3/8		2-3/8		2-3/8		2-3/8		2-3/8		2-3/8	
$h_{nom}$	(mm)	(60)		(60)		(60)		(60)		(60)		(60)	
Spacing (s) / edge distance (c <sub>e</sub> ) / concrete thickness (h) - in. (mm)	2 (51)	0.67		0.51		0.58		0.35		0.51		n/a	
	2-1/2 (64)	0.71		0.60		0.60		0.49		0.60		n/a	
	3 (76)	0.75		0.69		0.62		0.64		0.69		n/a	
	3-1/2 (89)	0.79		0.80		0.64		0.81		0.81		n/a	
	4 (102)	0.83		0.91		0.67		0.99		0.99		0.81	
	4-1/2 (114)	0.88		1.00		0.69		1.00		1.00		0.86	
	5 (127)	0.92				0.71						0.91	
	6 (152)	1.00				0.75						1.00	
	7 (178)					0.79							
	8 (203)					0.83							
	9 (229)					0.87							
	10 (254)					0.91							
	11 (279)					0.95							
	12 (305)					1.00							
14 (356)													

**Table 16 - Load adjustment factors for 1/2-in. diameter Hilti KWIK Bolt 3 stainless steel anchor in uncracked concrete<sup>1,2</sup>**

1/2-in. KB3 stainless steel uncracked concrete		Spacing factor in tension				Edge distance factor in tension				Spacing factor in shear <sup>3</sup>				Edge distance in shear				Concrete thickness factor in shear <sup>4</sup>		
		⊥ toward edge		to and away from edge																
		$f_{AN}$		$f_{RN}$		$f_{AV}$		$f_{RV}$		$f_{RV}$		$f_{RV}$		$f_{RV}$		$f_{HV}$				
Embedment	in.	2-1/4		3-1/2		2-1/4		3-1/2		2-1/4		3-1/2		2-1/4		3-1/2				
$h_{nom}$	(mm)	(57)		(89)		(57)		(89)		(57)		(89)		(57)		(89)				
Spacing (s) / edge distance (c <sub>e</sub> ) / concrete thickness (h) - in. (mm)	1-5/8 (41)	n/a		n/a		0.39		n/a		n/a		0.07		n/a		0.15		n/a		
	2 (51)	n/a		n/a		0.42		n/a		n/a		0.10		n/a		0.20		n/a		
	2-1/8 (54)	n/a		0.61		0.43		n/a		0.54		0.11		n/a		0.22		n/a		
	2-1/2 (64)	0.71		0.63		0.54		0.47		0.61		0.55		0.53		0.14		0.54		
	3 (76)	0.75		0.65		0.62		0.52		0.63		0.55		0.70		0.19		0.70		
	3-1/2 (89)	0.79		0.68		0.72		0.57		0.65		0.56		0.88		0.23		0.88		
	4 (102)	0.83		0.71		0.82		0.62		0.68		0.57		1.00		0.29		1.00		
	4-1/2 (114)	0.88		0.73		0.92		0.68		0.70		0.58		0.34		0.68		0.89		
	5 (127)	0.92		0.76		1.00		0.74		0.72		0.59		0.40		0.74		0.94		
	6 (152)	1.00		0.81			0.89		0.76		0.61		0.53		0.89		1.00		0.66	
	7 (178)			0.86			1.00		0.81		0.63		0.66		1.00				0.71	
	8 (203)			0.91					0.85		0.64		0.81						0.76	
	9 (229)			0.96					0.89		0.66		0.97						0.81	
	10 (254)			1.00					0.94		0.68		1.00						0.85	
	11 (279)								0.98		0.70								0.89	
	12 (305)								1.00		0.72								0.93	
	14 (356)										0.75								1.00	
	16 (406)										0.79									
	18 (457)										0.83									
	20 (508)										0.86									
> 24 (610)										0.93										

1 Linear interpolation not permitted.  
2 When combining multiple load adjustment factors (e.g. for a 4 anchor pattern in a corner with thin concrete member) the design can become very conservative. To optimize the design, use Hilti PROFIS Anchor Design software or perform anchor calculation using design equations from ACI 318-14 Chapter 17.  
3 Spacing factor reduction in shear,  $f_{AV}$ , assumes an influence of a nearby edge. If no edge exists, then  $f_{AV} = f_{AN}$ .  
4 Concrete thickness reduction factor in shear,  $f_{HV}$ , assumes an influence of a nearby edge. If no edge exists, then  $f_{HV} = 1.0$ .  
 If a reduction factor value is in a shaded cell, this indicates that this specific edge distance may not be permitted with a certain spacing (or vice versa). Check with table 13 and figure 3 of this section to calculate permissible edge distance, spacing and concrete thickness combinations. Use of Hilti KWIK Bolt 3 anchors with edge distance and spacing dimensions smaller than what is noted in this table is permitted.

Table 17 - Load adjustment factors for 5/8-in. diameter Hilti KWIK Bolt 3 stainless steel anchor in uncracked concrete<sup>1,2</sup>

5/8-in. KB3 stainless steel uncracked concrete		Spacing factor in tension $f_{AN}$		Edge distance factor in tension $f_{RN}$		Spacing factor in shear <sup>3</sup> $f_{AV}$		Edge distance in shear				Concrete thickness factor in shear <sup>4</sup> $f_{HV}$	
								⊥ toward edge $f_{RV}$		to and away from edge $f_{RV}$			
Embedment $h_{nom}$	in. (mm)	3-1/2 (89)	4-3/8 (111)	3-1/2 (89)	4-3/8 (111)	3-1/2 (89)	4-3/8 (111)	3-1/2 (89)	4-3/8 (111)	3-1/2 (89)	4-3/8 (111)	3-1/2 (89)	4-3/8 (111)
Spacing (s) / edge distance ( $c_e$ ) / concrete thickness (h) - in. (mm)	2-1/8 (54)	n/a	0.59	n/a	n/a	n/a	0.53	n/a	n/a	n/a	n/a	n/a	n/a
	2-1/2 (64)	n/a	0.60	n/a	0.37	n/a	0.54	n/a	0.12	n/a	0.23	n/a	n/a
	3 (76)	n/a	0.63	n/a	0.40	n/a	0.55	n/a	0.15	n/a	0.30	n/a	n/a
	3-1/8 (79)	0.67	0.63	n/a	0.41	0.56	0.55	n/a	0.16	n/a	0.32	n/a	n/a
	3-1/4 (83)	0.67	0.64	0.49	0.42	0.56	0.55	0.24	0.17	0.47	0.34	n/a	n/a
	3-1/2 (89)	0.69	0.65	0.51	0.44	0.57	0.56	0.26	0.19	0.51	0.38	n/a	n/a
	4 (102)	0.71	0.67	0.56	0.47	0.58	0.56	0.32	0.23	0.56	0.47	n/a	n/a
	5 (127)	0.77	0.71	0.68	0.55	0.60	0.58	0.45	0.33	0.68	0.55	0.63	n/a
	6 (152)	0.82	0.75	0.81	0.63	0.62	0.59	0.59	0.43	0.81	0.63	0.69	0.62
	7 (178)	0.87	0.79	0.95	0.74	0.64	0.61	0.75	0.54	0.95	0.74	0.74	0.67
	8 (203)	0.93	0.83	1.00	0.84	0.66	0.63	0.91	0.66	1.00	0.84	0.79	0.71
	9 (229)	0.98	0.88		0.95	0.68	0.64	1.00	0.79		0.95	0.84	0.75
	10 (254)	1.00	0.92		1.00	0.70	0.66		0.92		1.00	0.89	0.80
	11 (279)		0.96			0.72	0.67		1.00			0.93	0.83
	12 (305)		1.00			0.74	0.69					0.97	0.87
	14 (356)					0.77	0.72					1.00	0.94
	16 (406)					0.81	0.75						1.00
	18 (457)					0.85	0.78						
	20 (508)					0.89	0.82						
	24 (610)					0.97	0.88						
> 30 (762)					1.00	0.97							

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Table 18 - Load adjustment factors for 3/4-in. diameter Hilti KWIK Bolt 3 stainless steel anchor in uncracked concrete<sup>1,2</sup>

3/4-in. KB3 stainless steel uncracked concrete		Spacing factor in tension $f_{AN}$		Edge distance factor in tension $f_{RN}$		Spacing factor in shear <sup>3</sup> $f_{AV}$		Edge distance in shear				Concrete thickness factor in shear <sup>4</sup> $f_{HV}$	
								⊥ toward edge $f_{RV}$		to and away from edge $f_{RV}$			
Embedment $h_{nom}$	in. (mm)	4-1/4 (108)	5-1/2 (140)	4-1/4 (108)	5-1/2 (140)	4-1/4 (108)	5-1/2 (140)	4-1/4 (108)	5-1/2 (140)	4-1/4 (108)	5-1/2 (140)	4-1/4 (108)	5-1/2 (140)
Spacing (s) / edge distance ( $c_e$ ) / concrete thickness (h) - in. (mm)	2-7/8 (73)	n/a	n/a	n/a	0.43	n/a	n/a	n/a	0.11	n/a	0.23	n/a	n/a
	3 (76)	n/a	n/a	n/a	0.44	n/a	n/a	n/a	0.12	n/a	0.24	n/a	n/a
	3-1/4 (83)	n/a	n/a	0.37	0.46	n/a	n/a	0.20	0.14	0.37	0.27	n/a	n/a
	3-1/2 (89)	n/a	0.62	0.39	0.47	n/a	0.55	0.22	0.15	0.39	0.30	n/a	n/a
	4 (102)	0.68	0.63	0.42	0.51	0.57	0.55	0.27	0.18	0.42	0.37	n/a	n/a
	4-1/2 (114)	0.70	0.65	0.45	0.54	0.58	0.56	0.32	0.22	0.45	0.44	n/a	n/a
	5 (127)	0.72	0.67	0.49	0.58	0.59	0.57	0.38	0.26	0.49	0.52	n/a	n/a
	6 (152)	0.77	0.70	0.57	0.65	0.60	0.58	0.49	0.34	0.57	0.65	0.65	n/a
	7 (178)	0.81	0.73	0.67	0.73	0.62	0.59	0.62	0.43	0.67	0.73	0.70	n/a
	8 (203)	0.86	0.77	0.76	0.82	0.64	0.61	0.76	0.52	0.76	0.82	0.75	0.66
	9 (229)	0.90	0.80	0.86	0.92	0.66	0.62	0.91	0.62	0.91	0.92	0.79	0.70
	10 (254)	0.94	0.83	0.95	1.00	0.67	0.64	1.00	0.73	1.00	1.00	0.83	0.74
	11 (279)	0.99	0.87	1.00		0.69	0.65		0.84			0.87	0.77
	12 (305)	1.00	0.90			0.71	0.66		0.96			0.91	0.81
	14 (356)		0.97			0.74	0.69		1.00			0.99	0.87
	16 (406)		1.00			0.78	0.72					1.00	0.93
	18 (457)					0.81	0.74						0.99
	20 (508)					0.85	0.77						1.00
	24 (610)					0.92	0.82						
	30 (762)					1.00	0.91						
> 36 (914)						0.99							

- Linear interpolation not permitted.
- When combining multiple load adjustment factors (e.g. for a 4 anchor pattern in a corner with thin concrete member) the design can become very conservative. To optimize the design, use Hilti PROFIS Anchor Design software or perform anchor calculation using design equations from ACI 318-14 Chapter 17.
- Spacing factor reduction in shear,  $f_{AV}$ , assumes an influence of a nearby edge. If no edge exists, then  $f_{AV} = f_{AN}$ .
- Concrete thickness reduction factor in shear,  $f_{HV}$ , assumes an influence of a nearby edge. If no edge exists, then  $f_{HV} = 1.0$ .

☐ If a reduction factor value is in a shaded cell, this indicates that this specific edge distance may not be permitted with a certain spacing (or vice versa). Check with table 13 and figure 3 of this section to calculate permissible edge distance, spacing and concrete thickness combinations. Use of Hilti KWIK Bolt 3 anchors with edge distance and spacing dimensions smaller than what is noted in this table is permitted.

**Table 19 - Load adjustment factors for 1-in. diameter Hilti KWIK Bolt 3 stainless steel anchor in uncracked concrete<sup>1,2</sup>**

1-in. KB3 stainless steel uncracked concrete		Spacing factor in tension $f_{AN}$		Edge distance factor in tension $f_{RN}$		Spacing factor in shear <sup>3</sup> $f_{AV}$		Edge distance in shear				Concrete thickness factor in shear <sup>4</sup> $f_{HV}$	
								⊥ toward edge $f_{RV}$		to and away from edge $f_{RV}$			
								4-1/2 (114)	6-1/4 (159)	4-1/2 (114)	6-1/4 (159)		
Embedment $h_{nom}$	in. (mm)	4-1/2 (114)	6-1/4 (159)	4-1/2 (114)	6-1/4 (159)	4-1/2 (114)	6-1/4 (159)	4-1/2 (114)	6-1/4 (159)	4-1/2 (114)	6-1/4 (159)	4-1/2 (114)	6-1/4 (159)
Spacing (s) / edge distance ( $c_e$ ) / concrete thickness (h) - in. (mm)	3 (76)	n/a	n/a	n/a	0.43	n/a	n/a	n/a	0.10	n/a	0.20	n/a	n/a
	3-1/2 (89)	n/a	n/a	0.42	0.45	n/a	n/a	0.21	0.12	0.42	0.25	n/a	n/a
	4 (102)	n/a	n/a	0.45	0.48	n/a	n/a	0.26	0.15	0.45	0.30	n/a	n/a
	4-1/2 (114)	n/a	n/a	0.49	0.51	n/a	n/a	0.31	0.18	0.49	0.36	n/a	n/a
	4-3/4 (121)	n/a	0.64	0.50	0.53	n/a	0.56	0.34	0.20	0.50	0.39	n/a	n/a
	5 (127)	0.71	0.64	0.52	0.54	0.59	0.56	0.37	0.21	0.52	0.43	n/a	n/a
	6 (152)	0.75	0.67	0.60	0.60	0.60	0.57	0.48	0.28	0.60	0.56	n/a	n/a
	7 (178)	0.79	0.70	0.70	0.67	0.62	0.58	0.61	0.35	0.70	0.67	n/a	n/a
	8 (203)	0.83	0.73	0.80	0.74	0.64	0.60	0.74	0.43	0.80	0.74	0.74	n/a
	9 (229)	0.88	0.76	0.90	0.82	0.65	0.61	0.89	0.51	0.90	0.82	0.78	n/a
	10 (254)	0.92	0.79	1.00	0.91	0.67	0.62	1.00	0.60	1.00	0.91	0.83	0.69
	11 (279)	0.96	0.82		1.00	0.69	0.63		0.69		1.00	0.87	0.72
	12 (305)	1.00	0.85			0.70	0.64		0.79			0.91	0.76
	14 (356)		0.91			0.74	0.67		1.00			0.98	0.82
	16 (406)		0.96			0.77	0.69					1.00	0.87
	18 (457)		1.00			0.81	0.71						0.92
	20 (508)					0.84	0.74						0.98
	24 (610)					0.91	0.79						1.00
30 (762)					1.00	0.86							
> 36 (914)						0.93							

1 Linear interpolation not permitted.

2 When combining multiple load adjustment factors (e.g. for a 4 anchor pattern in a corner with thin concrete member) the design can become very conservative. To optimize the design, use Hilti PROFIS Anchor Design software or perform anchor calculation using design equations from ACI 318-14 Chapter 17.

3 Spacing factor reduction in shear,  $f_{AV}$ , assumes an influence of a nearby edge. If no edge exists, then  $f_{AV} = f_{AN}$ .

4 Concrete thickness reduction factor in shear,  $f_{HV}$ , assumes an influence of a nearby edge. If no edge exists, then  $f_{HV} = 1.0$ .

     If a reduction factor value is in a shaded cell, this indicates that this specific edge distance may not be permitted with a certain spacing (or vice versa). Check with table 13 and figure 3 of this section to calculate permissible edge distance, spacing and concrete thickness combinations. Use of Hilti KWIK Bolt 3 anchors with edge distance and spacing dimensions smaller than what is noted in this table is permitted.

**Table 20 - Hilti KWIK Bolt 3 hot-dip galvanized design strength with concrete/pullout failure in uncracked concrete<sup>1,2,3,4,5</sup>**

Nominal anchor diameter in.	Effective embed. in. (mm)	Nominal embed. in. (mm)	Tension - $\phi N_n$				Shear - $\phi V_n$			
			$f'_c = 2,500$ psi lb (kN)	$f'_c = 3,000$ psi lb (kN)	$f'_c = 4,000$ psi lb (kN)	$f'_c = 6,000$ psi lb (kN)	$f'_c = 2,500$ psi lb (kN)	$f'_c = 3,000$ psi lb (kN)	$f'_c = 4,000$ psi lb (kN)	$f'_c = 6,000$ psi lb (kN)
1/2	2 (51)	2-1/4 (57)	2,205 (9.8)	2,415 (10.7)	2,790 (12.4)	3,420 (15.2)	2,375 (10.6)	2,605 (11.6)	3,005 (13.4)	3,680 (16.4)
	3-1/4 (83)	3-1/2 (89)	4,250 (18.9)	4,655 (20.7)	5,375 (23.9)	6,585 (29.3)	9,845 (43.8)	10,785 (48.0)	12,450 (55.4)	15,250 (67.8)
5/8	3-1/8 (79)	3-1/2 (89)	4,200 (18.7)	4,605 (20.5)	5,315 (23.6)	6,510 (29.0)	9,280 (41.3)	10,165 (45.2)	11,740 (52.2)	14,380 (64.0)
	4 (102)	4-3/8 (111)	5,860 (26.1)	6,420 (28.6)	7,415 (33.0)	9,080 (40.4)	13,440 (59.8)	14,725 (65.5)	17,000 (75.6)	20,820 (92.6)
3/4	3-3/4 (95)	4-1/4 (108)	5,665 (25.2)	6,205 (27.6)	7,165 (31.9)	8,775 (39.0)	12,200 (54.3)	13,365 (59.5)	15,430 (68.6)	18,900 (84.1)
	5 (127)	5-1/2 (140)	6,615 (29.4)	7,245 (32.2)	8,365 (37.2)	10,245 (45.6)	18,785 (83.6)	20,575 (91.5)	23,760 (105.7)	29,100 (129.4)

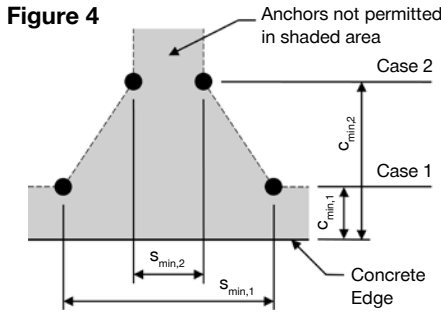
- 1 See section 3.1.8 to convert design strength value to ASD value.
- 2 Linear interpolation between embedment depths and concrete compressive strengths is not permitted.
- 3 Apply spacing, edge distance, and concrete thickness factors in tables 23 to 25 as necessary. Compare to steel values in table 21. The lesser of the values is to be used for the design.
- 4 Tabular values are for normal-weight concrete only. For lightweight concrete multiply design strength by  $\lambda_s$  as follows: for sand-lightweight,  $\lambda = 0.68$ ; for all-lightweight,  $\lambda = 0.60$
- 5 Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete.

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**Table 21 - Steel design strength for Hilti KWIK Bolt 3 hot-dip galvanized anchors<sup>1,2</sup>**

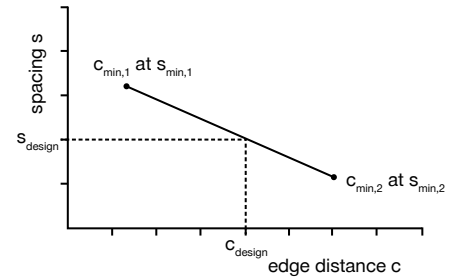
Nominal anchor diameter in.	Nominal embedment in. (mm)	Tensile $\phi N_{sa}$ <sup>3</sup> lb (kN)	Shear $\phi V_{sa}$ <sup>4</sup> lb (kN)
1/2	2-1/4 (57)	8,745 (38.9)	2,925 (13.0)
	3-1/2 (89)		3,815 (17.0)
5/8	3-1/2 (89)	13,515 (60.1)	7,565 (33.7)
	4-3/8 (111)		
3/4	4-1/4 (108)	19,080 (84.9)	11,050 (49.2)
	5-1/2 (140)		

- 1 See section 3.1.8 to convert design strength value to ASD value.
- 2 KWIK Bolt 3 carbon steel anchors are to be considered ductile steel elements.
- 3 Tensile  $\phi N_{sa} = \phi A_{se,N} f_{uta}$  as noted in ACI 318-14 Chapter 17.
- 4 Shear values determined by static shear tests with  $\phi V_{sa} < \phi 0.60 A_{se,V} f_{uta}$  as noted in ACI 318-14 Chapter 17.



For a specific edge distance, the permitted spacing is calculated as follows:

$$s \geq s_{\min,2} + \frac{(s_{\min,1} - s_{\min,2})}{(c_{\min,1} - c_{\min,2})} (c - c_{\min,2})$$



**Table 22 - Hot-dip galvanized KWIK Bolt 3 installation parameters<sup>1</sup>**

Setting information	Symbol	Units	Nominal anchor diameter d <sub>o</sub>											
			1/2		5/8		3/4							
Effective minimum embedment	<i>h<sub>ef</sub></i>	in. (mm)	2 (51)		3-1/4 (83)		3-1/8 (79)		4 (102)		3-3/4 (95)		5 (127)	
Minimum member thickness	<i>h<sub>min</sub></i>	in. (mm)	4 (102)	6 (152)	6 (152)	8 (203)	5 (127)	6 (152)	8 (203)	6 (152)	8 (203)	6 (152)	8 (203)	8 (203)
Case 1	<i>c<sub>min,1</sub></i>	in. (mm)	3-1/4 (83)	2-5/8 (67)	2 (51)		2-1/4 (57)	2 (51)	1-7/8 (48)	3-1/2 (89)		3-5/8 (92)		
	for <i>s<sub>min,1</sub></i> ≥	in. (mm)	6-1/4 (158)	5-1/2 (140)	4-7/8 (124)		5-1/4 (133)	5 (127)	4-3/4 (121)	7-1/2 (191)		7-3/8 (187)		
Case 2	<i>c<sub>min,2</sub></i>	in. (mm)	3-3/4 (95)	2-3/4 (70)	2-5/8 (67)	2-1/4 (57)	3-1/2 (89)	2-1/2 (64)	2-1/4 (57)	6-1/2 (165)		4-3/4 (121)		
	for <i>s<sub>min,2</sub></i> ≥	in. (mm)	3-1/8 (79)	2-3/4 (70)	2-3/8 (60)	2-1/8 (54)	2-1/2 (64)	2-1/8 (54)	2-1/8 (54)	4 (102)		3-7/8 (98)		

<sup>1</sup> Linear interpolation is permitted to establish an edge distance and spacing combination between Case 1 and Case 2. Linear interpolation for a specific edge distance *c*, where *c<sub>min,1</sub>* < *c* < *c<sub>min,2</sub>* will determine the permissible spacings.

**Table 23 - Load adjustment factors for 1/2-in. diameter Hilti KWIK Bolt 3 hot-dip galvanized anchor in uncracked concrete<sup>1,2</sup>**

1/2-in. KB3 hot-dip galvanized uncracked concrete	spacing factor in tension		edge distance factor in tension		spacing factor in shear <sup>3</sup>		Edge distance in shear				Conc. thickness factor in shear <sup>4</sup>		
	<i>f<sub>AN</sub></i>	<i>f<sub>RN</sub></i>	<i>f<sub>AV</sub></i>	<i>f<sub>RN</sub></i>	<i>f<sub>AV</sub></i>	<i>f<sub>RV</sub></i>	<i>f<sub>RV</sub></i>	<i>f<sub>RV</sub></i>	<i>f<sub>RV</sub></i>	<i>f<sub>HV</sub></i>	<i>f<sub>HV</sub></i>		
Embedment <i>h<sub>nom</sub></i>	in. (mm)	2-1/4 (57)	3-1/2 (89)	2-1/4 (57)	3-1/2 (89)	2-1/4 (57)	3-1/2 (89)	2-1/4 (57)	3-1/2 (89)	2-1/4 (57)	3-1/2 (89)	2-1/4 (57)	3-1/2 (89)
Spacing (s) / edge distance (c <sub>o</sub> ) / concrete thickness (h) - in. (mm)	2 (51)	n/a	n/a	n/a	0.38	n/a	n/a	n/a	0.10	n/a	0.20	n/a	n/a
	2-3/8 (60)	n/a	0.62	n/a	0.41	n/a	0.54	n/a	0.13	n/a	0.26	n/a	n/a
	2-1/2 (64)	n/a	0.63	n/a	0.42	n/a	0.55	n/a	0.14	n/a	0.28	n/a	n/a
	3 (76)	n/a	0.65	n/a	0.46	n/a	0.55	n/a	0.19	n/a	0.37	n/a	n/a
	3-1/8 (79)	0.76	0.66	n/a	0.48	0.64	0.56	n/a	0.20	n/a	0.40	n/a	n/a
	3-1/4 (83)	0.77	0.67	0.67	0.49	0.64	0.56	0.79	0.21	0.79	0.42	n/a	n/a
	3-1/2 (89)	0.79	0.68	0.72	0.51	0.65	0.56	0.88	0.23	0.88	0.47	n/a	n/a
	4 (102)	0.83	0.71	0.82	0.56	0.68	0.57	1.00	0.29	1.00	0.56	0.84	n/a
	4-1/2 (114)	0.88	0.73	0.92	0.61	0.70	0.58		0.34		0.61	0.89	n/a
	5 (127)	0.92	0.76	1.00	0.67	0.72	0.59		0.40		0.67	0.94	n/a
	6 (152)	1.00	0.81		0.80	0.76	0.61		0.53		0.80	1.00	0.66
	7 (178)	1.00	0.86		0.93	0.81	0.63		0.66		0.93		0.71
	8 (203)		0.91		1.00	0.85	0.64		0.81		1.00		0.76
	9 (229)		0.96			0.89	0.66		0.97				0.81
	10 (254)		1.00			0.94	0.68		1.00				0.85
	11 (279)					0.98	0.70						0.89
	12 (305)					1.00	0.72						0.93
	14 (356)						0.75						1.00
	16 (406)						0.79						
18 (457)						0.83							
20 (508)						0.86							
> 24 (610)						0.93							

<sup>1</sup> Linear interpolation not permitted.  
<sup>2</sup> When combining multiple load adjustment factors (e.g. for a 4 anchor pattern in a corner with thin concrete member) the design can become very conservative. To optimize the design, use Hilti PROFIS Anchor Design software or perform anchor calculation using design equations from ACI 318-14 Chapter 17.  
<sup>3</sup> Spacing factor reduction in shear, *f<sub>AV</sub>*, assumes an influence of a nearby edge. If no edge exists, then *f<sub>AV</sub>* = *f<sub>AN</sub>*.  
<sup>4</sup> Concrete thickness reduction factor in shear, *f<sub>HV</sub>*, assumes an influence of a nearby edge. If no edge exists, then *f<sub>HV</sub>* = 1.0.  
 If a reduction factor value is in a shaded cell, this indicates that this specific edge distance may not be permitted with a certain spacing (or vice versa). Check with table 22 and figure 4 of this section to calculate permissible edge distance, spacing and concrete thickness combinations. Use of Hilti KWIK Bolt 3 anchors with edge distance and spacing dimensions smaller than what is noted in this table is permitted.



**Table 24 - Load adjustment factors for 5/8-in. diameter Hilti KWIK Bolt 3 hot-dip galvanized anchor in uncracked concrete<sup>1,2</sup>**

5/8-in. KB3 hot-dip galvanized uncracked concrete		Spacing factor in tension $f_{AN}$		Edge distance factor in tension $f_{RN}$		Spacing factor in shear <sup>3</sup> $f_{AV}$		Edge distance in shear				Conc. thickness factor in shear <sup>4</sup> $f_{HV}$	
								⊥ toward edge $f_{RV}$		to and away from edge $f_{RV}$			
Embedment $h_{nom}$	in. (mm)	3-1/2 (89)	4-3/8 (111)	3-1/2 (89)	4-3/8 (111)	3-1/2 (89)	4-3/8 (111)	3-1/2 (89)	4-3/8 (111)	3-1/2 (89)	4-3/8 (111)	3-1/2 (89)	4-3/8 (111)
Spacing (s) / edge distance (c <sub>g</sub> ) / concrete thickness (h) - in. (mm)	2 (51)	n/a	n/a	n/a	0.34	n/a	n/a	n/a	0.08	n/a	0.17	n/a	n/a
	2-1/8 (54)	n/a	0.59	n/a	0.34	n/a	0.53	n/a	0.09	n/a	0.18	n/a	n/a
	2-1/4 (57)	n/a	0.59	0.38	0.35	n/a	0.54	0.14	0.10	0.27	0.20	n/a	n/a
	2-1/2 (64)	0.63	0.60	0.41	0.37	0.55	0.54	0.16	0.12	0.32	0.23	n/a	n/a
	3 (76)	0.66	0.63	0.45	0.40	0.56	0.55	0.21	0.15	0.42	0.30	n/a	n/a
	3-1/2 (89)	0.69	0.65	0.50	0.44	0.57	0.56	0.26	0.19	0.50	0.38	n/a	n/a
	4 (102)	0.71	0.67	0.54	0.47	0.58	0.56	0.32	0.23	0.54	0.47	n/a	n/a
	4-1/2 (114)	0.74	0.69	0.60	0.51	0.59	0.57	0.38	0.28	0.60	0.51	n/a	n/a
	5 (127)	0.77	0.71	0.66	0.55	0.60	0.58	0.45	0.33	0.66	0.55	0.63	n/a
	6 (152)	0.82	0.75	0.79	0.63	0.62	0.59	0.59	0.43	0.79	0.63	0.69	0.62
	7 (178)	0.87	0.79	0.92	0.74	0.64	0.61	0.75	0.54	0.92	0.74	0.74	0.67
	8 (203)	0.93	0.83	1.00	0.84	0.66	0.63	0.91	0.66	1.00	0.84	0.79	0.71
	9 (229)	0.98	0.88		0.95	0.68	0.64	1.00	0.79		0.95	0.84	0.75
	10 (254)	1.00	0.92		1.00	0.70	0.66		0.92		1.00	0.89	0.80
	11 (279)		0.96			0.72	0.67		1.00			0.93	0.83
	12 (305)		1.00			0.74	0.69					0.97	0.87
	14 (356)					0.77	0.72					1.00	0.94
	16 (406)					0.81	0.75						1.00
	18 (457)					0.85	0.78						
	20 (508)					0.89	0.82						
24 (610)					0.97	0.88							
> 30 (762)					1.00	0.97							

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**Table 25 - Load adjustment factors for 3/4-in. diameter Hilti KWIK Bolt 3 hot-dip galvanized anchor in uncracked concrete<sup>1,2</sup>**

3/4-in. KB3 hot-dip galvanized uncracked concrete		Spacing factor in tension $f_{AN}$		Edge distance factor in tension $f_{RN}$		Spacing factor in shear <sup>3</sup> $f_{AV}$		Edge distance in shear				Conc. thickness factor in shear <sup>4</sup> $f_{HV}$	
								⊥ toward edge $f_{RV}$		to and away from edge $f_{RV}$			
Embedment $h_{nom}$	in. (mm)	4-1/4 (108)	5-1/2 (140)	4-1/4 (108)	5-1/2 (140)	4-1/4 (108)	5-1/2 (140)	4-1/4 (108)	5-1/2 (140)	4-1/4 (108)	5-1/2 (140)	4-1/4 (108)	5-1/2 (140)
Spacing (s) / edge distance (c <sub>g</sub> ) / concrete thickness (h) - in. (mm)	3-1/2 (89)	n/a	n/a	0.41	n/a	n/a	n/a	0.22	n/a	0.41	n/a	n/a	n/a
	3-5/8 (92)	n/a	n/a	0.42	0.49	n/a	n/a	0.23	0.16	0.42	0.32	n/a	n/a
	3-7/8 (98)	n/a	0.63	0.44	0.51	n/a	0.55	0.26	0.18	0.44	0.35	n/a	n/a
	4 (102)	0.68	0.63	0.45	0.52	0.57	0.55	0.27	0.18	0.45	0.37	n/a	n/a
	4-1/2 (114)	0.70	0.65	0.49	0.56	0.58	0.56	0.32	0.22	0.49	0.44	n/a	n/a
	5 (127)	0.72	0.67	0.53	0.59	0.59	0.57	0.38	0.26	0.53	0.52	n/a	n/a
	5-1/2 (140)	0.74	0.68	0.57	0.63	0.60	0.57	0.43	0.30	0.57	0.60	n/a	n/a
	6 (152)	0.77	0.70	0.62	0.67	0.60	0.58	0.49	0.34	0.62	0.67	0.65	n/a
	7 (178)	0.81	0.73	0.72	0.75	0.62	0.59	0.62	0.43	0.72	0.75	0.70	n/a
	8 (203)	0.86	0.77	0.82	0.84	0.64	0.61	0.76	0.52	0.82	0.84	0.75	0.66
	9 (229)	0.90	0.80	0.92	0.95	0.66	0.62	0.91	0.62	0.92	0.95	0.79	0.70
	10 (254)	0.94	0.83	1.00	1.00	0.67	0.64	1.00	0.73	1.00	1.00	0.83	0.74
	11 (279)	0.99	0.87			0.69	0.65		0.84			0.87	0.77
	12 (305)	1.00	0.90			0.71	0.66		0.96			0.91	0.81
	14 (356)		0.97			0.74	0.69		1.00			0.99	0.87
	16 (406)		1.00			0.78	0.72					1.00	0.93
	18 (457)					0.81	0.74						0.99
	20 (508)					0.85	0.77						1.00
	24 (610)					0.92	0.82						
	30 (762)					1.00	0.91						
> 36 (914)						0.99							

- Linear interpolation not permitted.
  - When combining multiple load adjustment factors (e.g. for a 4 anchor pattern in a corner with thin concrete member) the design can become very conservative. To optimize the design, use Hilti PROFIS Anchor Design software or perform anchor calculation using design equations from ACI 318-14 Chapter 17.
  - Spacing factor reduction in shear,  $f_{AV}$ , assumes an influence of a nearby edge. If no edge exists, then  $f_{AV} = f_{AN}$ .
  - Concrete thickness reduction factor in shear,  $f_{HV}$ , assumes an influence of a nearby edge. If no edge exists, then  $f_{HV} = 1.0$ .
- ☐ If a reduction factor value is in a shaded cell, this indicates that this specific edge distance may not be permitted with a certain spacing (or vice versa). Check with table 22 and figure 4 of this section to calculate permissible edge distance, spacing and concrete thickness combinations. Use of Hilti KWIK Bolt 3 anchors with edge distance and spacing dimensions smaller than what is noted in this table is permitted.

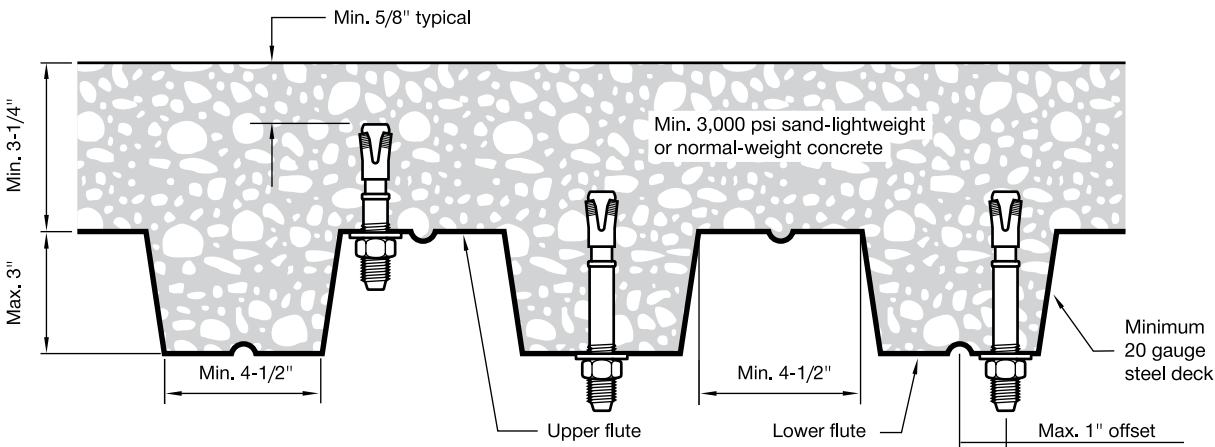
**Table 26 - Hilti KWIK Bolt 3 carbon steel design strength in the soffit of uncracked lightweight concrete over metal deck<sup>1,2,3,4,5,6,8</sup>**

Nominal anchor diameter in.	Effective embed. in. (mm)	Nominal embed. in. (mm)	Loads according to figure 5			
			Tension - $\phi N_n$		Shear - $\phi V_n$	
			$f'_c = 3,000$ psi lb (kN)	$f'_c = 4,000$ psi lb (kN)	$f'_c = 3,000$ psi lb (kN)	$f'_c = 4,000$ psi lb (kN)
1/4	1-1/2 (38)	1-3/4 (44)	1,140 (5.1)	1,315 (5.8)	1,255 (5.6)	1,255 (5.6)
3/8	2 (51)	2-3/8 (60)	1,460 (6.5)	1,685 (7.5)	1,845 (8.2)	1,845 (8.2)
1/2	2 (51)	2-1/4 (57)	1,775 (7.9)	2,050 (9.1)	2,050 (9.1)	2,050 (9.1)
	3-1/4 (83)	3-1/2 (89)				
5/8	3-1/8 (79)	3-1/2 (89)	3,095 (13.8)	3,575 (15.9)	4,280 (19.0)	4,280 (19.0)
	4 (102)	4-3/8 (111)				

**Table 27 - Hilti KWIK Bolt 3 stainless steel design strength in the soffit of uncracked lightweight concrete over metal deck<sup>1,2,3,4,5,7,8</sup>**

Nominal anchor diameter in.	Effective embed. in. (mm)	Nominal embed. in. (mm)	Loads according to figure 5			
			Tension - $\phi N_n$		Shear - $\phi V_n$	
			$f'_c = 3,000$ psi lb (kN)	$f'_c = 4,000$ psi lb (kN)	$f'_c = 3,000$ psi lb (kN)	$f'_c = 4,000$ psi lb (kN)
1/4	1-1/2 (38)	1-3/4 (44)	1,175 (5.2)	1,355 (6.0)	1,315 (5.8)	1,315 (5.8)
3/8	2 (51)	2-3/8 (60)	1,675 (7.5)	1,935 (8.6)	1,675 (7.5)	1,675 (7.5)
1/2	2 (51)	2-1/4 (57)	1,265 (5.6)	1,460 (6.5)	1,135 (5.0)	1,135 (5.0)
	3-1/4 (83)	3-1/2 (89)				
5/8	3-1/8 (79)	3-1/2 (89)	2,880 (12.8)	3,325 (14.8)	3,700 (16.5)	3,700 (16.5)
	4 (102)	4-3/8 (111)				

- 1 See section 3.1.8 to convert design strength value to ASD value.
- 2 Linear interpolation between embedment depths and concrete compressive strengths is not permitted.
- 3 Tabular value is for one anchor per flute. Minimum spacing along the length of the flute is  $3 \times h_{ef}$  (effective embedment).
- 4 Tabular values are lightweight concrete and no additional reduction factor is needed.
- 5 No additional reduction factors for spacing or edge distance need to be applied.
- 6 Comparison to steel values in table 4 is not required. Values in tables 26 control.
- 7 Comparison to steel values in table 12 is not required. Values in tables 27 control.
- 8 Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete.



**Figure 5 - Installation in concrete over metal deck**

## DESIGN INFORMATION IN CONCRETE PER CSA A23.3

Limit State Design of anchors is described in the provisions of CSA A23.3-14 Annex D for post-installed anchors tested and assessed in accordance with ACI 355.2 for mechanical anchors and ACI 355.4 for adhesive anchors. This section contains the Limit State Design tables with unfactored characteristic loads that are based on the published loads in ICC Evaluation Services ESR-2302. These tables are followed by factored resistance tables. The factored resistance tables have characteristic design loads that are prefactored by the applicable reduction factors for a single anchor with no anchor-to-anchor spacing or edge distance adjustments for the convenience of the user of this document. All the figures in the previous ACI 318-14 Chapter 17 design section are applicable to Limit State Design and the tables will reference these figures.

For a detailed explanation of the tables developed in accordance with CSA A23.3-14 Annex D, refer to Section 3.1.8. Technical assistance is available by contacting Hilti Canada at (800) 363-4458 or at [www.hilti.com](http://www.hilti.com).

**Table 28 - Steel resistance for Hilti KWIK Bolt 3 carbon steel anchors<sup>1,2</sup>** 

Nominal anchor diameter in.	Nominal embedment in. (mm)	Tensile $N_{sar}$ <sup>3</sup> lb (kN)	Shear $V_{sar}$ <sup>4</sup> lb (kN)
1/4	1-11/16 (43)	1,440 (6.4)	1,045 (4.6)
3/8	2-3/8 (60)	4,325 (19.2)	2,850 (12.7)
1/2	2-1/4 (57)	7,930 (35.3)	4,230 (18.8)
	3-1/2 (89)		4,305 (19.1)
5/8	3-1/2 (89)	12,255 (54.5)	7,795 (34.7)
	4-3/8 (111)		
3/4	4-1/4 (108)	17,300 (77.0)	9,985 (44.4)
	5-1/2 (140)		10,580 (47.1)

- 1 See Section 3.1.8 to convert factored resistance value to ASD value.
- 2 Hilti KWIK Bolt 3 carbon steel anchors are to be considered ductile steel elements.
- 3 Tensile  $N_{sar} = A_{se,N} \phi_s f_{uta} R$  as noted in CSA A23.3-14 Annex D.
- 4 Shear determined by static shear tests with  $V_{sar} < A_{se,V} \phi_s 0.6 f_{uta} R$  as noted in CSA A23.3-14 Annex D.

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**Table 29 - Hilti KWIK Bolt 3 carbon steel design information in accordance with CSA A23.3-14 Annex D<sup>1</sup>**


Design parameter	Symbol	Units	Nominal anchor diameter												Ref		
			1/4	3/8	1/2		5/8		3/4								
Anchor O.D.	$d_a$	in. (mm)	0.25 (6.4)	0.375 (9.5)	0.5 (12.7)		0.625 (15.9)		0.75 (19.1)								A23.3-14
Effective minimum embedment <sup>2</sup>	$h_{ef}$	in. (mm)	1-1/2 (38)	2 (51)		2 (51)		3-1/4 (83)		3-1/8 (79)		4 (102)		3-3/4 (95)		5 (127)	
Minimum concrete thickness <sup>3</sup>	$h_{min}$	in. (mm)	4 (102)	4 (102)	5 (127)	4 (102)	6 (152)	6 (152)	8 (203)	5 (127)	6 (152)	8 (203)	6 (152)	8 (203)	8 (203)		
Critical edge distance	$c_{ac}$	in. (mm)	2-3/4 (70)	4-1/2 (114)	3-7/8 (98)	4-7/8 (124)	3-5/8 (92)	6-3/4 (171)	5-5/8 (143)	7-1/2 (191)	9-1/2 (241)	7-1/2 (191)	9-3/4 (248)	7-1/2 (191)	9-1/2 (241)		
Minimum edge distance	$c_{min}$	in. (mm)	1-3/8 (35)	2 (51)	1-1/2 (38)	2-1/8 (54)	2 (51)	1-5/8 (41)	1-5/8 (41)	2-1/4 (57)	1-3/4 (44)	1-3/4 (44)	2-3/4 (70)	2-5/8 (67)	2-1/2 (64)		
	for $s >$	in. (mm)	1-3/4 (44)	2-7/8 (73)	3-1/2 (89)	4-7/8 (124)	4-3/4 (121)	4-1/4 (108)	4 (102)	5-1/4 (133)	4-3/4 (121)	4 (102)	6-7/8 (175)	6-1/2 (165)	6-3/8 (162)		
Minimum anchor spacing	$s_{min}$	in. (mm)	1-1/4 (32)	1-3/4 (44)	1-3/4 (44)	2-1/2 (64)	2-1/4 (57)	2 (2)	1-7/8 (48)	2-3/8 (60)	2-1/8 (54)	2-1/8 (54)	3-3/4 (95)	3-3/8 (86)	2-1/2 (64)		
	for $c >$	in. (mm)	1-5/8 (41)	2-3/8 (60)	2-3/8 (60)	2-5/8 (67)	2-3/8 (60)	2-1/4 (57)	2 (51)	3-1/8 (79)	2-3/8 (60)	2-1/4 (57)	3-3/4 (95)	3-3/8 (86)	6-3/8 (162)		
Minimum hole depth in concrete	$h_o$	in. (mm)	2 (50.8)	2-5/8 (67)		2-5/8 (67)		4 (102)		3-7/8 (98)	4-3/4 (121)		4-1/2 (117)		5-3/4 (146)		
Minimum specified yield strength	$f_{ya}$	psi (N/mm <sup>2</sup> )	84,800 (585)	84,800 (585)		84,800 (585)		84,800 (585)		84,800 (585)		84,800 (585)		84,800 (585)			
Minimum specified ultimate strength	$f_{uta}$	psi (N/mm <sup>2</sup> )	106,000 (731)	106,000 (731)		106,000 (731)		106,000 (731)		106,000 (731)		106,000 (731)		106,000 (731)			
Effective tensile stress area	$A_{se,N}$	in <sup>2</sup> (mm <sup>2</sup> )	0.02 (12.9)	0.06 (38.7)		0.11 (71.0)		0.17 (109.7)		0.17 (109.7)		0.24 (154.8)		0.24 (154.8)			
Steel embedment material resistance factor for reinforcement	$\phi_s$	-	0.85												8.4.3		
Resistance modification factor for tension, steel failure modes <sup>3</sup>	R	-	0.80												D.5.3		
Resistance modification factor for shear, steel failure modes <sup>3</sup>	R	-	0.75												D.5.3		
Factored steel resistance in tension	$N_{sar}$	lb (kN)	1,440 (6.4)	4,325 (19.2)		7,930 (35.3)		12,255 (54.5)		12,255 (54.5)		17,300 (77.0)		17,300 (77.0)			D.6.1.2
Factored steel resistance in shear	$V_{sar}$	lb (kN)	1,045 (4.6)	2,850 (12.7)		4,230 (18.8)		4,305 (19.2)		7,795 (34.7)		9,985 (44.4)		10,580 (47.1)			D.7.1.2
Coeff. for factored concrete breakout resistance, uncracked concrete	$k_{c,uncr}$	-	10												D.6.2.2		
Modification factor for anchor resistance, tension, uncracked concrete <sup>4</sup>	$\psi_{c,N}$	-	1.0												D.6.2.6		
Anchor category	-	-	1												D.5.3 (c)		
Concrete material resistance factor	$\phi_c$	-	0.65												8.4.2		
Resistance modification factor for tension and shear, concrete failure modes, Condition B <sup>5</sup>	R	-	1.00												D.5.3 (c)		
Factored pullout resistance in 20 MPa uncracked concrete <sup>6</sup>	$N_{pr,uncr}$	lb (kN)	1,100 (4.9)	N/A		N/A		4,745 (21.1)		NA		NA		7,420 (33.0)			D.6.3.2

- Design information in this table is taken from ICC-ES ESR-2302, dated December 1, 2015, table 4, and converted for use with CSA A23.3-14 Annex D.
- See figure 1 of this section.
- The carbon steel KWIK Bolt 3 is considered a ductile steel element as defined by CSA A23.3-14 Annex D section D.2.
- For all design cases,  $\psi_{c,N} = 1.0$ . The appropriate coefficient for breakout resistance for uncracked concrete ( $k_{c,uncr}$ ) must be used.
- For use with the load combinations of CSA A23.3-14 chapter 8. Condition B applies where supplementary reinforcement in conformance with CSA A23.3-14 section D.5.3 is not provided, or where pullout or pryout strength governs. For cases where the presence of supplementary reinforcement can be verified, the resistance modification factors associated with Condition A may be used.
- For all design cases,  $\psi_{c,P} = 1.0$ . NA (not applicable) denotes that this value does not control for design. See section 4.1.4 of ESR-2302 for additional information.

**Table 30 - Hilti KWIK Bolt 3 carbon steel factored resistance with concrete/pullout failure in uncracked concrete<sup>1,2,3,4,5</sup>**

Nominal anchor diameter in.	Effective embed. in. (mm)	Nominal embed. in. (mm)	Tension - $N_r$				Shear - $V_r$			
			$f'_c = 20$ MPa (2,900psi) lb (kN)	$f'_c = 25$ MPa (3,625 psi) lb (kN)	$f'_c = 30$ MPa (4,350 psi) lb (kN)	$f'_c = 40$ MPa (5,800 psi) lb (kN)	$f'_c = 20$ MPa (2,900 psi) lb (kN)	$f'_c = 25$ MPa (3,625 psi) lb (kN)	$f'_c = 30$ MPa (4,350 psi) lb (kN)	$f'_c = 40$ MPa (5,800 psi) lb (kN)
1/4	1 1/2 (38)	1-11/16 43	1,100 (4.9)	1,230 (5.5)	1,350 (6.0)	1,560 (6.9)	1,530 (6.8)	1,710 (7.6)	1,875 (8.3)	2,165 (9.6)
3/8	2 (51)	2-5/16 (59)	2,380 (10.6)	2,660 (11.8)	2,915 (13.0)	3,365 (15.0)	2,380 (10.6)	2,660 (11.8)	2,915 (13.0)	3,365 (15.0)
1/2	2 (51)	2 3/8 (60)	2,380 (10.6)	2,660 (11.8)	2,915 (13.0)	3,365 (15.0)	2,380 (10.6)	2,660 (11.8)	2,915 (13.0)	3,365 (15.0)
	3-1/4 (83)	3 5/8 (92)	4,755 (21.1)	5,315 (23.6)	5,825 (25.9)	6,725 (29.9)	9,885 (44.0)	11,050 (49.2)	12,105 (53.8)	13,975 (62.2)
5/8	3-1/8 (79)	3-9/16 (90)	4,590 (20.4)	5,130 (22.8)	5,620 (25.0)	6,490 (28.9)	9,175 (40.8)	10,260 (45.6)	11,240 (50.0)	12,980 (57.7)
	4 (102)	4-7/16 (113)	6,730 (29.9)	7,525 (33.5)	8,245 (36.7)	9,520 (42.3)	13,465 (59.9)	15,055 (67.0)	16,490 (73.4)	19,040 (84.7)
3/4	3-3/4 (95)	4-5/16 (110)	6,050 (26.9)	6,765 (30.1)	7,410 (33.0)	8,555 (38.1)	12,100 (53.8)	13,530 (60.2)	14,820 (65.9)	17,115 (76.1)
	4-3/4 (121)	5-9/16 (141)	7,415 (33.0)	8,290 (36.9)	9,080 (40.4)	10,485 (46.6)	17,395 (77.4)	19,450 (86.5)	21,305 (94.8)	24,600 (109.4)

- See section 3.1.8 to convert factored resistance value to ASD value.
- Linear interpolation between embedment depths and concrete compressive strengths is not permitted.
- Apply spacing, edge distance, and concrete thickness factors in tables 6 to 10 as necessary. Compare to the steel values in table 28. The lesser of the values is to be used for the design.
- Tabular values are for normal-weight concrete only. For lightweight concrete multiply design strength by  $\lambda_a$  as follows: for sand-lightweight,  $\lambda_a = 0.68$ ; for all-lightweight,  $\lambda_a = 0.60$
- Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete.

**Table 31 - Steel resistance for Hilti KWIK Bolt 3 stainless steel anchors<sup>1,2</sup>**

Nominal anchor diameter in.	Nominal embedment in. (mm)	Tensile $N_{sar}$ <sup>3</sup> lb (kN)	Shear $V_{sar}$ <sup>4</sup> lb (kN)
1/4	1-11/16 (42.9)	1,565 (7.0)	1,070 (4.8)
3/8	2-3/8 (60.3)	4,690 (20.9)	3,175 (14.1)
1/2	2-1/4 (57.2)	8,600 (38.3)	2,675 (11.9)
	3-1/2 (88.9)		4,425 (19.7)
5/8	3-1/2 (88.9)	13,295 (59.1)	5,710 (25.4)
	4-3/8 (111.1)		9,115 (40.5)
3/4	4-1/4 (108.0)	14,690 (65.3)	7,585 (33.7)
	5-1/2 (139.7)		15,010 (66.8)
1	4-5/8 (117.5)	28,770 (128.0)	7,975 (35.5)
	5-7/8 (149.2)		17,430 (77.5)

- See Section 3.1.8 to convert factored resistance value to ASD value.
- Hilti KWIK Bolt 3 carbon steel anchors are to be considered ductile steel elements.
- Tensile  $N_{sar} = A_{se,N} \Phi_s f_{uta} R$  as noted in CSA A23.3-14 Annex D.
- Shear determined by static shear tests with  $V_{sar} < A_{se,V} \Phi_s 0.6 f_{uta} R$  as noted in CSA A23.3-14 Annex D.

**Table 32 - Hilti KWIK Bolt 3 stainless steel design information in accordance with CSA A23.3-14 Annex D<sup>1</sup>**


Design parameter	Symbol	Units	Nominal anchor diameter														Ref A23.3-14				
			1/4	3/8		1/2		5/8		3/4		1									
Anchor O.D.	$d_a$	in. (mm)	0.25 (6.4)	0.375 (9.5)		0.5 (12.7)		0.625 (15.9)		0.75 (19.1)		1 (25.4)									
Effective minimum embedment <sup>2</sup>	$h_{ef}$	in. (mm)	1-1/2 (38)	2 (51)		2 (51)		3-1/4 (83)		3-1/8 (79)		4 (102)		3-3/4 (95)		5 (127)		4 (102)		5-1/4 (133)	
Minimum concrete thickness <sup>2</sup>	$h_{min}$	in. (mm)	4 (102)	4 (102)	5 (127)	4 (102)	6 (152)	6 (152)	8 (203)	5 (127)	6 (152)	8 (203)	6 (152)	8 (203)	8 (203)	8 (203)	8 (203)	10 (254)			
Critical edge distance	$c_{ac}$	in. (mm)	3 (76)	4-3/8 (111)	3-7/8 (98)	4-7/8 (124)	4 (102)	6-3/4 (171)	5-3/4 (146)	7-3/8 (187)	9-1/2 (241)	7-1/2 (191)	10-1/2 (267)	9-1/4 (235)	9-3/4 (248)	10 (254)	11 (279)				
Minimum edge distance	$c_{min}$	in. (mm)	1-3/8 (35)	2 (51)	1-5/8 (41)	2-1/2 (64)	1.875 (48)	1-5/8 (41)	1-5/8 (41)	3-1/4 (83)	2-1/2 (64)	2-1/2 (64)	3-1/4 (83)	3 (76)	2-7/8 (73)	3-1/2 (89)	3 (76)				
	for $s >$	in. (mm)	1-3/4 (44)	4 (102)	3-3/8 (86)	5 (127)	4-5/8 (117)	4-1/2 (114)	4.25 (108)	5-5/8 (143)	5-1/4 (133)	5 (127)	7 (178)	6-7/8 (175)	6-5/8 (168)	6-3/4 (171)	6-3/4 (171)				
Minimum anchor spacing	$s_{min}$	in. (mm)	1-1/4 (32)	2 (51)	1-3/4 (44)	2-1/2 (64)	2-1/4 (57)	2 (51)	1-7/8 (48)	3-1/8 (79)	2-1/8 (54)	2-1/8 (54)	4 (102)	3-1/2 (89)	3-1/2 (89)	5 (127)	4-3/4 (121)				
	for $c >$	in. (mm)	1-5/8 (41)	3-1/4 (83)	2-1/2 (64)	2-7/8 (73)	2-3/8 (60)	2-3/8 (60)	2-1/8 (54)	3-7/8 (98)	3 (76)	2-3/4 (70)	4-1/8 (105)	3-3/4 (95)	3-3/4 (95)	4-1/4 (108)	3-3/4 (95)				
Minimum hole depth in concrete	$h_o$	in. (mm)	2 (50.8)	2-5/8 (67)		2-5/8 (67)		4 (102)		3-7/8 (98)		4-3/4 (121)		4-1/2 (117)		5-3/4 (146)		5 (127)		6-3/4 (165)	
Minimum specified yield strength	$f_{ya}$	psi (N/mm <sup>2</sup> )	84,800 (585)	92,000 (634)		92,000 (634)		92,000 (634)		92,000 (634)		76,000 (524)		76,000 (524)		76,000 (524)					
Minimum specified ultimate strength	$f_{uta}$	psi (N/mm <sup>2</sup> )	115,000 (793)	115,000 (793)		115,000 (793)		115,000 (793)		115,000 (793)		90,000 (621)		90,000 (621)		90,000 (621)					
Effective tensile stress area	$A_{se,N}$	in <sup>2</sup> (mm <sup>2</sup> )	0.02 (12.9)	0.06 (38.7)		0.11 (71.0)		0.17 (109.7)		0.17 (109.7)		0.24 (154.8)		0.24 (154.8)		0.47 (304.8)					
Steel embedment material resistance factor for reinforcement	$\phi_s$	-	0.85														8.4.3				
Resistance modification factor for tension, steel failure modes <sup>3</sup>	R	-	0.80														D.5.3				
Resistance modification factor for shear, steel failure modes <sup>3</sup>	R	-	0.75														D.5.3				
Factored steel resistance in tension	$N_{sar}$	lb (kN)	1,565 (7.0)	4,690 (20.9)		8,600 (38.3)		13,295 (59.1)		14,690 (65.3)		28,770 (128.0)		28,770 (128.0)		28,770 (128.0)		D.6.1.2			
Factored steel resistance in shear	$V_{sar}$	lb (kN)	1,070 (4.8)	3,175 (14.1)		2,675 (11.9)		4,425 (19.7)		5,710 (25.4)		9,115 (66.8)		7,585 (33.7)		15,010 (66.8)		7,975 (35.5)		17,430 (77.5)	
Coeff. for factored concrete breakout resistance, uncracked concrete	$k_{c,uncr}$	-	10														D.6.2.2				
Modification factor for anchor resistance, tension, uncracked concrete <sup>4</sup>	$\psi_{c,N}$	-	1.0														D.6.2.6				
Anchor category	-	-	2		1														D.5.3 (c)		
Concrete material resistance factor	$\phi_c$	-	0.65														8.4.2				
Resistance modification factor for tension and shear, concrete failure modes, Condition B <sup>5</sup>	R	-	0.85		1.00														D.5.3 (c)		
Factored pullout resistance in 20 MPa uncracked concrete <sup>6</sup>	$N_{pr,uncr}$	lb (kN)	1,100 (4.9)	2,070 (9.2)		2,315 (10.3)		4,225 (18.8)		4,360 (19.4)		5,485 (24.4)		6,000 (26.7)		7,600 (33.8)		NA		10,905 (48.5)	

1 Design information in this table is taken from ICC-ES ESR-2302, dated December 1, 2015, table 4, and converted for use with CSA A23.3-14 Annex D.  
2 See figure 1 of this section.  
3 The stainless steel KWIK Bolt 3 is considered a ductile steel element as defined by CSA A23.3-14 Annex D section D.2.  
4 For all design cases,  $\psi_{c,N} = 1.0$ . The appropriate coefficient for breakout resistance for uncracked concrete ( $k_{c,uncr}$ ) must be used.  
5 For use with the load combinations of CSA A23.3-14 chapter 8. Condition B applies where supplementary reinforcement in conformance with CSA A23.3-14 section D.5.3 is not provided, or where pullout or pryout strength governs. For cases where the presence of supplementary reinforcement can be verified, the resistance modification factors associated with Condition A may be used.  
6 For all design cases,  $\psi_{c,p} = 1.0$ . NA (not applicable) denotes that this value does not control for design. See section 4.1.4 of ESR-2302 for additional information.

**Table 33 - Hilti KWIK Bolt 3 stainless steel factored resistance with concrete/pullout failure in uncracked concrete<sup>1,2,3,4,5</sup>**

Nominal anchor diameter in.	Effective embed. in. (mm)	Nominal embed. in. (mm)	Tension - $N_r$				Shear - $V_r$			
			$f'_c = 20$ MPa (2,900psi) lb (kN)	$f'_c = 25$ MPa (3,625 psi) lb (kN)	$f'_c = 30$ MPa (4,350 psi) lb (kN)	$f'_c = 40$ MPa (5,800 psi) lb (kN)	$f'_c = 20$ MPa (2,900 psi) lb (kN)	$f'_c = 25$ MPa (3,625 psi) lb (kN)	$f'_c = 30$ MPa (4,350 psi) lb (kN)	$f'_c = 40$ MPa (5,800 psi) lb (kN)
1/4	1 1/2 (38)	1-11/16 43	930 (4.1)	1,040 (4.6)	1,140 (5.1)	1,315 (5.8)	1,300 (5.8)	1,455 (6.5)	1,595 (7.1)	1,840 (8.2)
3/8	2 (51)	2-5/16 (59)	2,080 (9.2)	2,325 (10.3)	2,545 (11.3)	2,940 (13.1)	2,380 (10.6)	2,660 (11.8)	2,915 (13.0)	3,365 (15.0)
1/2	2 (51)	2 3/8 (60)	2,315 (10.3)	2,585 (11.5)	2,835 (12.6)	3,275 (14.6)	2,380 (10.6)	2,660 (11.8)	2,915 (13.0)	3,365 (15.0)
	3-1/4 (83)	3 5/8 (92)	4,220 (18.8)	4,715 (21.0)	5,165 (23.0)	5,965 (26.5)	9,885 (44.0)	11,050 (49.2)	12,105 (53.8)	13,975 (62.2)
5/8	3-1/8 (79)	3-9/16 (90)	4,360 (19.4)	4,875 (21.7)	5,340 (23.8)	6,165 (27.4)	9,175 (40.8)	10,260 (45.6)	11,240 (50.0)	12,980 (57.7)
	4 (102)	4-7/16 (113)	5,480 (24.4)	6,125 (27.2)	6,710 (29.8)	7,750 (34.5)	13,465 (59.9)	15,055 (67.0)	16,490 (73.4)	19,040 (84.7)
3/4	3-3/4 (95)	4-5/16 (110)	6,000 (26.7)	6,705 (29.8)	7,345 (32.7)	8,480 (37.7)	12,100 (53.8)	13,530 (60.2)	14,820 (65.9)	17,115 (76.1)
	4-3/4 (121)	5-9/16 (141)	7,590 (33.8)	8,485 (37.7)	9,295 (41.3)	10,730 (47.7)	17,395 (77.4)	19,450 (86.5)	21,305 (94.8)	24,600 (109.4)
1	4 (102)	4-5/16 (110)	6,730 (29.9)	7,525 (33.5)	8,245 (36.7)	9,520 (42.3)	13,465 (59.9)	15,055 (67.0)	16,490 (73.4)	19,040 (84.7)
	5 3/4 (146)	5-9/16 (141)	10,895 (48.5)	12,180 (54.2)	13,340 (59.3)	15,405 (68.5)	23,055 (102.6)	25,780 (114.7)	28,240 (125.6)	32,610 (145.0)

- See section 3.1.8 to convert factored resistance value to ASD value.
- Linear interpolation between embedment depths and concrete compressive strengths is not permitted.
- Apply spacing, edge distance, and concrete thickness factors in tables 14 to 19 as necessary. Compare to the steel values in table 31. The lesser of the values is to be used for the design.
- Tabular values are for normal-weight concrete only. For lightweight concrete multiply design strength by  $\lambda_a$  as follows: for sand-lightweight,  $\lambda_a = 0.68$ ; for all-lightweight,  $\lambda_a = 0.60$
- Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete.

3.3.8

**Table 34 - Steel resistance for Hilti KWIK Bolt 3 hot-dip galvanized carbon steel anchors<sup>1,2</sup>**

Nominal anchor diameter in.	Nominal embedment in. (mm)	Tensile $N_{sar}$ <sup>3</sup> lb (kN)	Shear $V_{sar}$ <sup>4</sup> lb (kN)
1/2	2-1/4 (57)	7,930 (35.3)	2,870 (12.8)
	3-1/2 (89)		3,740 (16.6)
5/8	3-1/2 (89)	12,255 (54.5)	7,415 (33.0)
	4-3/8 (111)		
3/4	4-1/4 (108)	17,300 (77.0)	10,840 (48.2)
	5-1/2 (140)		

- See section 3.1.8 to convert design strength value to ASD value.
- KWIK Bolt 3 hot-dip galvanized carbon steel anchors are to be considered ductile steel elements.
- Tensile  $N_{sar} = A_{se,N} \phi_s f_{uta} R$  as noted in ACI 318-14 Chapter 17.
- Shear values determined by static shear tests with  $V_{sar} < A_{se,V} \phi_s 0.6 f_{uta} R$  as noted in ACI 318-14 Chapter 17.

**Table 35 - Hilti KWIK Bolt 3 hot-dip galvanized carbon steel design information in accordance with CSA A23.3-14 Annex D<sup>1</sup>**

Design parameter	Symbol	Units									Ref A23.3-14			
			1/2		5/8		3/4							
Anchor O.D.	$d_a$	in. (mm)	0.5 (12.7)		0.625 (15.9)		0.75 (19.1)							
Effective minimum embedment <sup>2</sup>	$h_{ef}$	in. (mm)	2 (51)		3-1/4 (83)		3-1/8 (79)		4 (102)		3-3/4 (95)	4-3/4 (121)		
Minimum concrete thickness	$h_{min}$	in. (mm)	4 (102)	6 (152)	6 (152)	8 (203)	5 (127)	6 (152)	8 (203)	6 (152)	8 (203)	8 (203)		
Critical edge distance	$c_{ac}$	in. (mm)	4-7/8 (124)	3-5/8 (92)	7-1/2 (191)	5.75 (146)	8 (194)	9-1/2 (241)	8 (197)	9-3/4 (248)	7-1/2 (191)	9-1/2 (241)		
Minimum edge distance	$c_{min}$	in. (mm)	2-7/8 (73)		2-1/8 (54)		3-1/4 (83)		2-3/8 (60)		4-1/4 (108)		4 (102)	
	for $s >$	in. (mm)	5-3/4 (146)		5-1/4 (133)		5-1/2 (140)		5-1/2 (140)		10 (254)		8-1/2 (216)	
Minimum anchor spacing	$s_{min}$	in. (mm)	2-7/8 (73)		2 (51)		2-3/4 (70)		2-3/8 (60)		5 (127)		4 (102)	
	for $c >$	in. (mm)	4-1/2 (114)		3-1/4 (83)		4-1/8 (105)		4-1/4 (108)		9-1/2 (241)		7 (178)	
Minimum hole depth in concrete	$h_o$	in. (mm)	2-5/8 (67)		4 (102)		3-3/4 (98)		4-3/4 (121)		4-1/2 (117)		5-3/4 (146)	
Minimum specified yield strength	$f_{ya}$	psi (N/mm <sup>2</sup> )	92,000 (634)		92,000 (634)		92,000 (634)		76,125 (525)					
Minimum specified ultimate strength	$f_{uta}$	psi (N/mm <sup>2</sup> )	115,000 (793)		115,000 (793)		115,000 (793)		101,500 (700)					
Effective tensile stress area	$A_{se,N}$	in <sup>2</sup> (mm <sup>2</sup> )	0.101 (65.0)		0.162 (104.6)		0.237 (152.8)							
Steel embedment material resistance factor for reinforcement	$\phi_s$	-			0.85								8.4.3	
Resistance modification factor for tension, steel failure modes <sup>4</sup>	R	-			0.80								D.5.3	
Resistance modification factor for shear, steel failure modes <sup>4</sup>	R	-			0.75								D.5.3	
Factored steel resistance in tension	$N_{sar}$	lb (kN)	7,930 (35.3)		12,255 (54.5)		17,300 (77.0)						D.6.1.2	
Factored steel resistance in shear	$V_{sar}$	lb (kN)	2,870 (12.8)		3,740 (16.6)		7,415 (33.0)		10,840 (48.2)				D.7.1.2	
Coefficient for factored concrete breakout resistance, uncracked concrete	$k_{c,uncr}$	-			10								D.6.2.2	
Modification factor for anchor resistance, tension, uncracked concrete <sup>4</sup>	$\psi_{c,N}$	-			1.00								D.6.2.6	
Anchor category	-	-			1								D.5.3 (c)	
Concrete material resistance factor	$\phi_c$	-			0.65								8.4.2	
Resistance modification factor for tension and shear, concrete failure modes, Condition B <sup>5</sup>	R	-			1.00								D.5.3 (c)	
Factored pullout resistance in 20 MPa uncracked concrete <sup>6</sup>	$N_{pr,uncr}$	lb (kN)	N/A		4,585 (20.4)		4,540 (20.2)		6,315 (28.1)		NA		7,125 (31.7)	D.6.3.2

- 1 Design information in this table is taken from ICC-ES ESR-2302, dated December 1, 2015, table 4, and converted for use with CSA A23.3-14 Annex D.
- 2 See figure 1 of this section.
- 3 The hot-dip galvanized carbon steel KWIK Bolt 3 is considered a ductile steel element as defined by CSA A23.3-14 Annex D section D.2.
- 4 For all design cases,  $\psi_{c,N} = 1.0$ . The appropriate coefficient for breakout resistance for uncracked concrete ( $k_{c,uncr}$ ) must be used.
- 5 For use with the load combinations of CSA A23.3-14 chapter 8. Condition B applies where supplementary reinforcement in conformance with CSA A23.3-14 section D.5.3 is not provided, or where pullout or pryout strength governs. For cases where the presence of supplementary reinforcement can be verified, the resistance modification factors associated with Condition A may be used.
- 6 For all design cases,  $\psi_{c,p} = 1.0$ . NA (not applicable) denotes that this value does not control for design. See section 4.1.4 of ESR-2302 for additional information.




**Table 36 - Hilti KWIK Bolt 3 hot-dip galvanized carbon steel factored resistance with concrete / pullout failure in uncracked concrete<sup>1,2,3,4,5</sup>**

Nominal anchor diameter in.	Effective embed. in. (mm)	Nominal embed. in. (mm)	Tension - $N_r$				Shear - $V_r$			
			$f'_c = 20$ MPa (2,900psi) lb (kN)	$f'_c = 25$ MPa (3,625 psi) lb (kN)	$f'_c = 30$ MPa (4,350 psi) lb (kN)	$f'_c = 40$ MPa (5,800 psi) lb (kN)	$f'_c = 20$ MPa (2,900 psi) lb (kN)	$f'_c = 25$ MPa (3,625 psi) lb (kN)	$f'_c = 30$ MPa (4,350 psi) lb (kN)	$f'_c = 40$ MPa (5,800 psi) lb (kN)
1/2	2 (51)	2 3/8 (60)	2,380 (10.6)	2,660 (11.8)	2,915 (13.0)	3,365 (15.0)	2,380 (10.6)	2,660 (11.8)	2,915 (13.0)	3,365 (15.0)
	3-1/4 (83)	3 5/8 (92)	4,580 (20.4)	5,120 (22.8)	5,610 (25.0)	6,480 (28.8)	9,885 (44.0)	11,050 (49.2)	12,105 (53.8)	13,975 (62.2)
5/8	3-1/8 (79)	3-9/16 (90)	4,535 (20.2)	5,070 (22.5)	5,555 (24.7)	6,410 (28.5)	9,175 (40.8)	10,260 (45.6)	11,240 (50.0)	12,980 (57.7)
	4 (102)	4-7/16 (113)	6,315 (28.1)	7,060 (31.4)	7,730 (34.4)	8,930 (39.7)	13,465 (59.9)	15,055 (67.0)	16,490 (73.4)	19,040 (84.7)
3/4	3-3/4 (95)	4-5/16 (110)	6,050 (26.9)	6,765 (30.1)	7,410 (33.0)	8,555 (38.1)	12,100 (53.8)	13,530 (60.2)	14,820 (65.9)	17,115 (76.1)
	4-3/4 (121)	5-9/16 (141)	7,130 (31.7)	7,975 (35.5)	8,735 (38.9)	10,085 (44.9)	17,395 (77.4)	19,450 (86.5)	21,305 (94.8)	24,600 (109.4)

- 1 See section 3.1.8 to convert factored resistance value to ASD value.
- 2 Linear interpolation between embedment depths and concrete compressive strengths is not permitted.
- 3 Apply spacing, edge distance, and concrete thickness factors in tables 23 to 25 as necessary. Compare to the steel values in table 34. The lesser of the values is to be used for the design.
- 4 Tabular values are for normal-weight concrete only. For lightweight concrete multiply design strength by  $\lambda_a$  as follows: for sand-lightweight,  $\lambda_a = 0.68$ ; for all-lightweight,  $\lambda_a = 0.60$
- 5 Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete.

3.3.8

**Table 37 - Hilti KWIK Bolt 3 carbon steel factored resistance in the soffit of uncracked lightweight concrete over metal deck<sup>1,2,3,4,5,6,7</sup>**

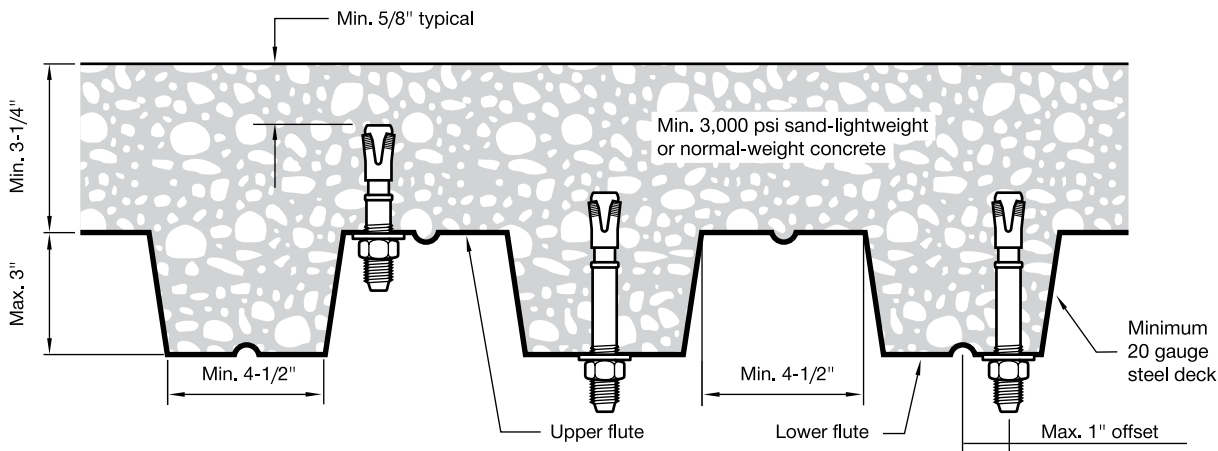

Nominal anchor diameter in.	Effective embed. in. (mm)	Nominal embed. in. (mm)	Loads according to figure 5		
			Tension - $N_r$		Shear - $V_r$
			$f'_c = 20$ MPa (2,900 psi) lb (kN)	$f'_c = 30$ MPa (4,350 psi) lb (kN)	$f'_c \geq 20$ MPa (2,900 psi) lb (kN)
1/4	1-1/2 (38)	1-11/16 (43)	1,120 (5.0)	1,370 (6.1)	1,230 (5.5)
3/8	2 (51)	2-5/16 (59)	1,435 (6.4)	1,755 (7.8)	1,810 (8.1)
1/2	2 (51)	2-3/8 (60)	1,745 (7.8)	2,135 (9.5)	2,010 (8.9)
	3-1/4 (83)	3-5/8 (92)			
5/8	3-1/8 (79)	3-9/16 (90)	3,045 (13.5)	3,730 (16.6)	4,200 (18.7)
	4 (102)	4-7/16 (113)			

- 1 See section 3.1.8 to convert design strength value to ASD value.
- 2 Linear interpolation between embedment depths and concrete compressive strengths is not permitted.
- 3 Tabular value is for one anchor per flute. Minimum spacing along the length of the flute is  $3 \times h_{ef}$  (effective embedment).
- 4 Tabular value is for lightweight concrete and no additional reduction factor is needed.
- 5 No additional reduction factors for spacing or edge distance need to be applied.
- 6 Comparison of the tabular values to the steel strength is not necessary. Tabular values control.
- 7 Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete.

**Table 38 - Hilti KWIK Bolt 3 stainless steel factored resistance in the soffit of uncracked lightweight concrete over metal deck**<sup>1,2,3,4,5,6,7</sup>

Nominal anchor diameter in.	Effective embed. in. (mm)	Nominal embed. in. (mm)	Loads according to figure 5		
			Tension - $N_t$		Shear - $V_r$
			$f'_c = 20$ MPa (2,900 psi) lb (kN)	$f'_c = 30$ MPa (4,350 psi) lb (kN)	$f'_c \geq 20$ MPa (2,900 psi) lb (kN)
1/4	1-1/2 (38)	1-11/16 (43)	980 (4.4)	1,200 (5.3)	1,290 (5.7)
3/8	2 (51)	2-5/16 (59)	1,650 (7.3)	2,020 (9.0)	1,645 (7.3)
1/2	2 (51)	2-3/8 (60)	1,245 (5.5)	1,520 (6.8)	1,110 (4.9)
	3-1/4 (83)	3-5/8 (92)			
5/8	3-1/8 (79)	3-9/16 (90)	2,830 (12.6)	3,465 (15.4)	3,625 (16.1)
	4 (102)	4-7/16 (113)			

- 1 See section 3.1.8 to convert design strength value to ASD value.
- 2 Linear interpolation between embedment depths and concrete compressive strengths is not permitted.
- 3 Tabular value is for one anchor per flute. Minimum spacing along the length of the flute is  $3 \times h_{ef}$  (effective embedment).
- 4 Tabular value is for lightweight concrete and no additional reduction factor is needed.
- 5 No additional reduction factors for spacing or edge distance need to be applied.
- 6 Comparison of the tabular values to the steel strength is not necessary. Tabular values control.
- 7 Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete.



**Figure 5 - Installation in concrete over metal deck**

DESIGN INFORMATION IN MASONRY

Table 39 - Carbon steel Hilti KWIK Bolt 3 allowable loads in grout-filled concrete masonry units<sup>1, 2, 3, 4, 5, 6</sup>

Nominal anchor diameter in.	Nominal embedment		Minimum distance from edge of wall		Tension		Shear lb (kN)	
	in.	(mm)	in.	(mm)	lb	(kN)	lb	(kN)
1/4	1-1/8	(29)	4	(102)	150	(0.7)	380	(1.7)
			12	(305)				
	2	(51)	4	(102)	540	(2.4)	445	(2.0)
			12	(305)				
3/8	1-5/8	(41)	4	(102)	320	(1.4)	735	(3.3)
			12	(305)				
	2-1/2	(64)	4	(102)	780	(3.5)	1,010	(4.5)
			12	(305)			1,395	(6.2)
1/2	2-1/4	(57)	4	(102)	630	(2.8)	830	(3.7)
			12	(305)				
	3-1/2	(89)	4	(102)	905	(4.0)	1,080	(4.8)
			12	(305)			2,375	(10.6)
5/8	2-3/4	(70)	4	(102)	815	(3.6)	890	(4.0)
			12	(305)				
	4	(102)	4	(102)	1,240	(5.5)	970	(4.3)
			12	(305)				
3/4	3-1/4	(83)	4	(102)	1,035	(4.6)	785	(3.5)
			12	(305)			3,135	(13.8)
	4-3/4	(121)	4	(102)	1,645	(7.3)	825	(3.7)
			12	(305)				

3.3.8

Table 40 - Carbon steel Hilti KWIK Bolt 3 allowable loads for anchors installed in top of grout-filled concrete masonry wall<sup>1</sup>

Nominal anchor diameter in.	Nominal embedment		Tension		Shear			
	in.	(mm)	lb	(kN)	V <sub>1</sub>		V <sub>2</sub>	
			lb	(kN)	lb	(kN)	lb	(kN)
1/2	3	(76)	645	(2.9)	310	(1.4)	615	(2.7)
5/8	3-1/2	(89)	850	(3.8)	310	(1.4)	615	(2.7)

- 1 All values are for anchors installed in fully grouted concrete masonry with minimum masonry prism strength of 1,500 psi. Concrete masonry units may be lightweight, medium-weight or normal-weight conforming to ASTM C90. Allowable loads are calculated using safety factor of 4.
- 2 Anchors must be installed a minimum of 1-3/8 inch from any vertical mortar joint.
- 3 Anchor locations are limited to one per masonry cell.
- 4 Embedment depth is measured from the outside face of the concrete masonry unit.
- 5 Linear interpolation to determine load values at intermediate edge distances is permitted.

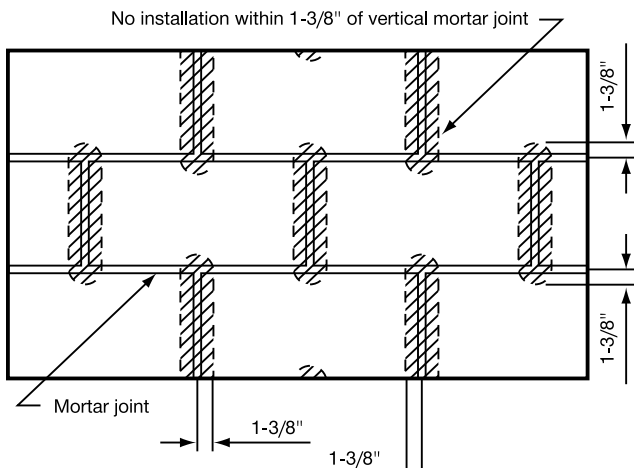


Figure 6 - Installation in grout-filled concrete masonry unit

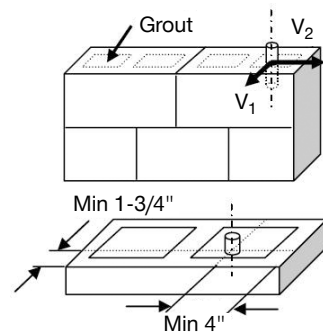


Figure 7 - Hilti KWIK Bolt 3 installed in the top of masonry walls

## DESIGN INFORMATION FOR COUNTERSUNK KWIK BOLT 3

**Table 41 - Countersunk Hilti KWIK Bolt 3 allowable loads in normal-weight concrete<sup>1</sup>**

Anchor Material	Nominal anchor diameter in.	Embedment depth in. (mm)		$f'_c = 3000 \text{ psi (20.7 MPa)}$			
				Tension lb (kN)		Shear <sup>2</sup> lb (kN)	
Carbon Steel	1/4	1-1/8	(29)	365	(1.6)	350	(1.6)
	3/8	1-5/8	(41)	810	(3.6)	750	(3.3)
Stainless Steel	1/4	1-1/8	(29)	320	(1.4)	500	(2.2)
	3/8	1-5/8	(41)	670	(3.0)	1330	(5.9)

1 Allowable loads based on using a safety factor of 4.0.

2 Shear values acting thru threads of anchor bolt. If acting through the empty shell, reduce loads by 70%.

## INSTALLATION INSTRUCTIONS

Installation Instructions For Use (IFU) are included with each product package. They can also be viewed or downloaded online at [www.hilti.com](http://www.hilti.com). Because of the possibility of changes, always verify that downloaded IFU are current when used. Proper installation is critical to achieve full performance. Training is available on request. Contact Hilti Technical Services for applications and conditions not addressed in the IFU.



## ORDERING INFORMATION

## KWIK Bolt 3 anchor product line

Size	Length (ℓ)		Thread length (ℓ <sub>th</sub> )		ID stamp	Box	Carbon steel	304 SS	316 SS	HDG
	in.	(mm)	in.	(mm)						
1/4 x 1-3/4	1-3/4	(44)	3/4	(18)	A	100	●	●		
1/4 x 2-1/4	2-1/4	(57)	7/8	(22)	B		●	●	●	
1/4 x 3-1/4	3-1/4	(83)	2	(51)	D		●	●		
			7/8	(22)					●	
1/4 x 4-1/2	4-1/2	(114)	2-7/8	(75)	G		●	●		
3/8 x 2-1/4	2-1/4	(57)	7/8	(22)	B	50	●	●		
3/8 x 3	3	(76)	1-1/4	(32)	D				●	
			1-1/2	(40)			●	●		
3/8 x 3-3/4	3-3/4	(95)	1-1/4	(32)	E				●	
			2-1/4	(59)			●	●		
3/8 x 5	5	(127)	3-1/2	(91)	H	●	●			
3/8 x 7	7	(178)	5-1/2	(142)	L	●	●			
1/2 x 2-3/4	2-3/4	(70)	1-1/4	(33)	C	25	●	●		
1/2 x 3-3/4	3-3/4	(95)	1-5/16	(35)	E				●	
			2-3/16	(56)			●	●		●
1/2 x 4-1/2	4-1/2	(114)	1-5/16	(35)	G				●	
			2-7/8	(75)			●	●		●
1/2 x 5-1/2	5-1/2	(140)	1-5/16	(35)	I			●		
			3-3/4	(96)		●	●		●	
1/2 x 7	7	(178)	4-3/4	(121)	L	●	●		●	
5/8 x 3-3/4	3-3/4	(95)	1-1/2	(41)	E	15	●	●	●	
5/8 x 4-3/4	4-3/4	(121)	1-1/2	(41)	G				●	
			2-3/4	(70)			●	●		●
5/8 x 6	6	(152)	1-1/2	(41)	J				●	
			4	(102)			●	●		●
5/8 x 7	7	(178)	4-3/4	(121)		●	●			
5/8 x 8-1/2	8-1/2	(216)	6-1/2	(166)	O	●	●			
5/8 x 10	10	(254)	7	(180)	R	●	●			
3/4 x 4-3/4	4-3/4	(121)	1-1/2	(41)	G	20		●	●	
			2-7/16	(62)		10	●			●
						20		●		
3/4 x 5-1/2	5-1/2	(140)	1-1/2	(41)	I	20		●		
			3-7/16	(85)		10	●			●
						20		●		
3/4 x 7	7	(178)	4-5/8	(119)	L	10	●			
			4-7/8	(124)				●		
3/4 x 8	8	(203)	5-3/4	(146)	N		●	●		●
3/4 x 10	10	(254)	5-7/8	(152)	R		●	●	●	
3/4 x 12	12	(305)	5-7/8	(152)	T		●	●		
1 x 6	6	(152)	2-1/4	(57)	J	5	●	●	●	
1 x 9	9	(114)	2-1/4	(57)	P		●	●		
1 x 12	12	(114)	6	(152)	T		●	●		

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### Countersunk KWIK Bolt 3 anchor product line

Size	Length		Box	Carbon steel	304 SS
	in.	(mm)			
C1/4 x 2	2	(51)	100	•	
C1/4 x 3	3	(76)	100	•	•
C1/4 x 5	5	(127)	100	•	
C3/8 x 2-1/4	2-1/4	(57)	100	•	
C3/8 x 3	3	(76)	100	•	
C3/8 x 4	4	(102)	50	•	•
C3/8 x 5	5	(127)	50	•	

### Rod Coupling KWIK Bolt 3 anchor product line

Size	Length		Thread length		ID stamp	Box quantity
	in.	(mm)	in.	(mm)		
3/8 x 2-1/4	2-1/4	(57)	7/8	(22)	B	100

### HHDCA ceiling anchor product line

Size	Length		Eyelet size in.	Box quantity
	in.	(mm)		
1/4 x 2	2-1/32	(52)	5/16	100

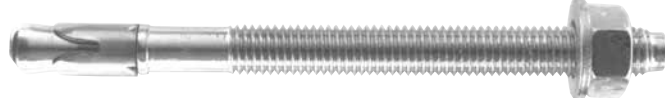
**KWIK Bolt 3 anchor**



**Rod coupling KWIK Bolt 3 anchor 3/8 x 2 1/4**



**Long thread KWIK Bolt 3 anchor**



**HHDCA ceiling hanger 1/4 x 2**



**Countersunk KWIK Bolt 3 anchor**



**Table 43 - KWIK Bolt 3 length identification system**

Length ID marking on bolt head	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W
Length of anchor, $l_{\text{anch}}$ in.	From 1 1/2	2	2 1/2	3	3 1/2	4	4 1/2	5	5 1/2	6	6 1/2	7	7 1/2	8	8 1/2	9	9 1/2	10	11	12	13	14	15
Up to but not including	2	2 1/2	3	3 1/2	4	4 1/2	5	5 1/2	6	6 1/2	7	7 1/2	8	8 1/2	9	9 1/2	10	11	12	13	14	15	16